

WMG-4

Advances in Computational Modeling and Materials Characterization for the Microwave Power Industry

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¹QWED Sp. z o. o.



IMS Booth #2537

*Special thanks to Lukasz Nowicki,
QWED's new team member and PhD student at the Warsaw Univ. Tech.,
for his assistance in assembling this presentation.*

- Motivation & Background:
 - Digital Twin & Its Applications
 - **The Bases & Timeline of QWED Research**
- Computational Physics-Based Modeling of Microwave Heating
- Experimental Acquisition of Material Parameters
- Conclusions

Computer Aided Design of microwave power systems requires having a “twin” of the physical reality:

Physics Equations

(PE)

Maxwell, heat flow, fluid flow, load movement,
...

Material relations

(MR)

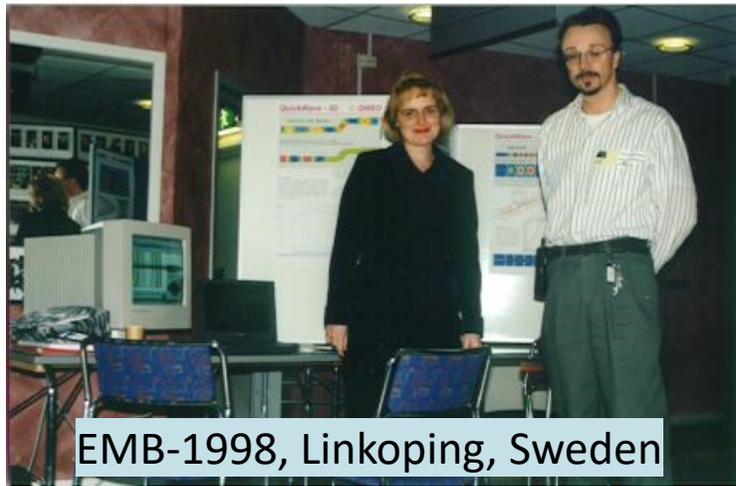
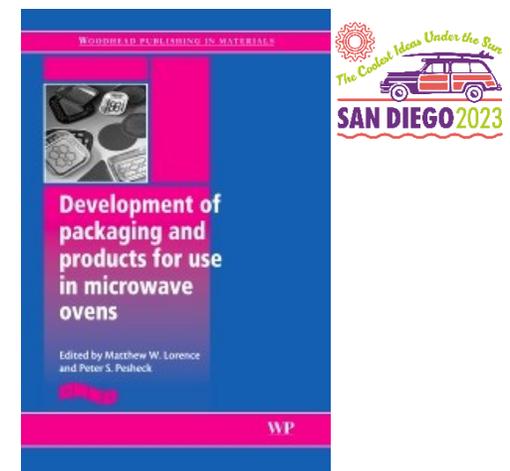
literature data or own measurements

Our team has been active in both areas for over 26 years!

QuickWave™ software

GHz-resonator-based instruments

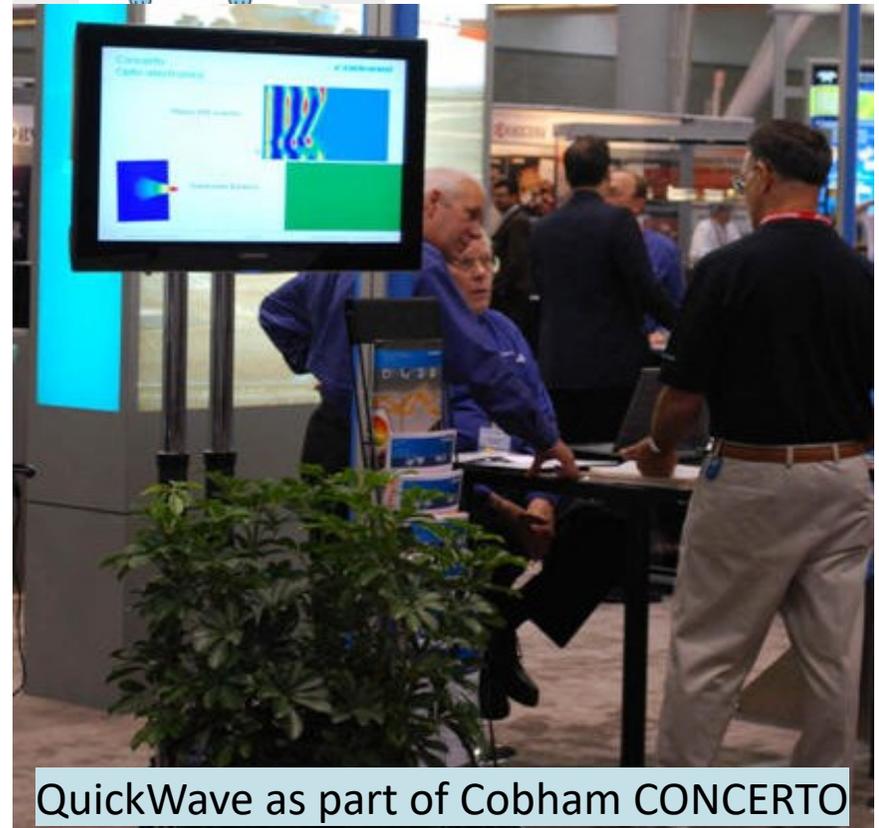
Modeling of MW Heating: Our Early Days



EMB-1998, Linkoping, Sweden



IEEE IMS 1999, Anaheim, CA

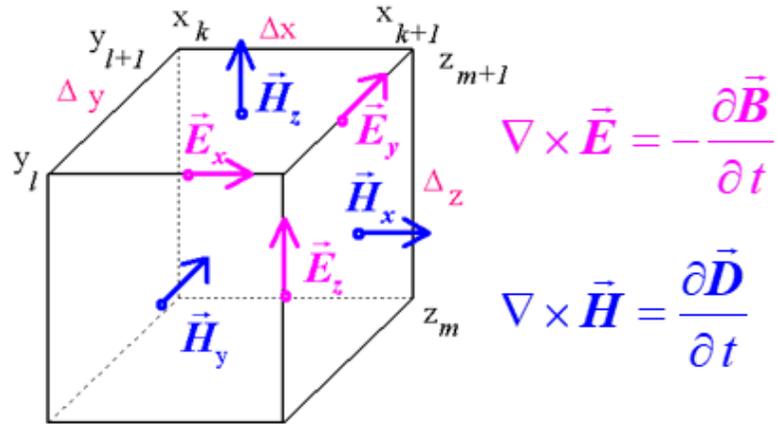


QuickWave as part of Cobham CONCERTO



IEEE IMS 2014, Tampa, FL

FDTD (Finite-Difference Time-Domain Method): explicit, **fast**, emulates natural physical processes

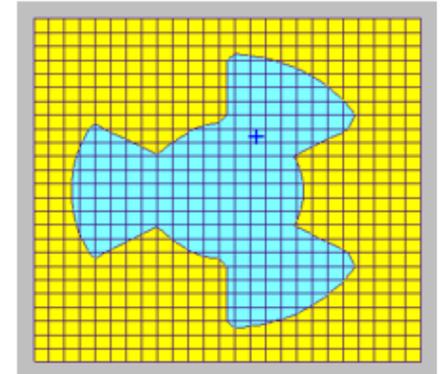
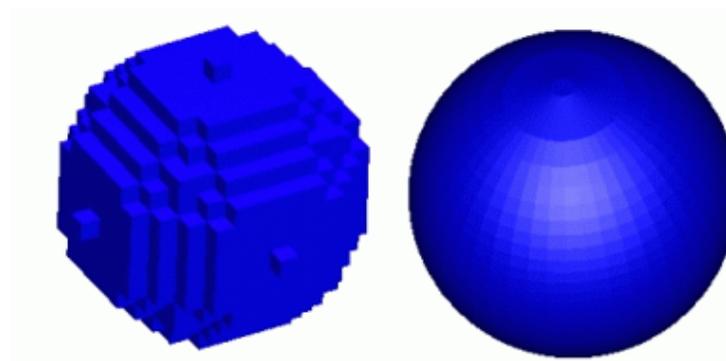
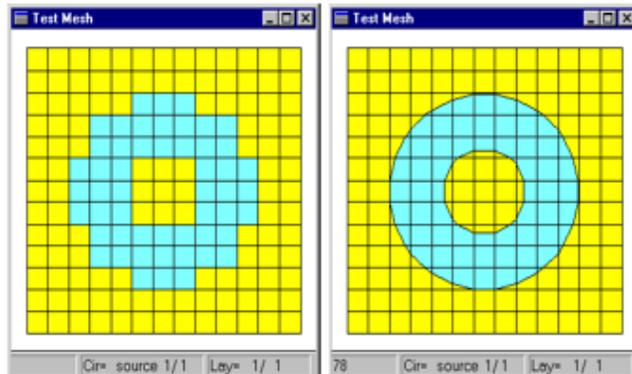
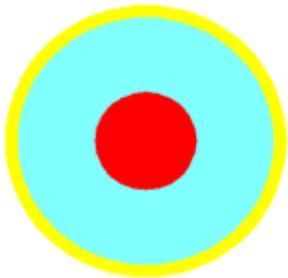


$${}_{k,l,m+0.5}E_z^n = E_z(x_k, y_l, z_m + 0.5\Delta z, t_0 + n\Delta t)$$

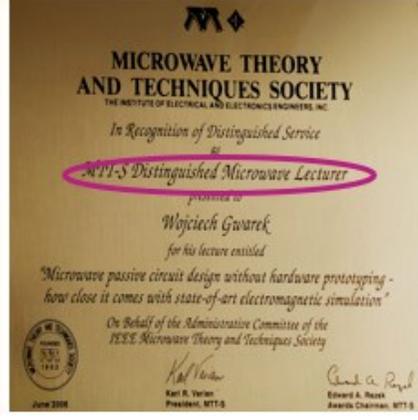
$${}_{k,l,m+0.5}E_z^{n+1} = E_z^n + \frac{\Delta t}{{}_{k,l,m+0.5}\epsilon_z \epsilon_0} \cdot \left\{ \left[{}_{k+0.5,l,m+0.5}H_y^{n+0.5} - {}_{k-0.5,l,m+0.5}H_y^{n+0.5} \right] \frac{1}{\Delta x} + \left[{}_{k,l-0.5,m+0.5}H_x^{n+0.5} - {}_{k,l+0.5,m+0.5}H_x^{n+0.5} \right] \frac{1}{\Delta y} \right\}$$

"Keep an eye on this one, it promises to be a gem",
Mark Mirotznik,
IEEE Spectrum April 1998

We discretise time and space (in a conformal manner).



IEEE- awarded research of **Prof. Wojciech Gwarek**,
 QWED's co-founder (1997) & 1st President (till 2017)



New conformal FDTD method:

- + Conformal Space Discretisation (similar to FEM - arbitrary shapes).
- + Time-Domain Solution (faster than FEM - wide frequency band, diagonal mass matrices).

TRANSACTIONS ON MICROWAVE THEORY AND TECHNIQUES, VOL. MTT-33, NO. 10, OCTOBER 1985 1067

Analysis of an Arbitrarily-Shaped Planar Circuit—A Time-Domain Approach

WOJCIECH K. GWAREK
(Invited Paper)

$$\nabla V(x, y, t) = -L_s \frac{\partial J(x, y, t)}{\partial t}$$

$$\nabla \cdot J(x, y, t) = -C_s \frac{\partial V(x, y, t)}{\partial t}$$

IEEE TRANSACTIONS ON MICROWAVE THEORY AND TECHNIQUES, VOL. 36, NO. 2, FEBRUARY 1988

Computer-Aided Analysis of Arbitrarily Shaped Coaxial Discontinuities

WOJCIECH K. GWAREK

738

Analysis of Arbitrarily Shaped Two-Dimensional Microwave Circuits by Finite-Difference Time-Domain Method

WOJCIECH K. GWAREK

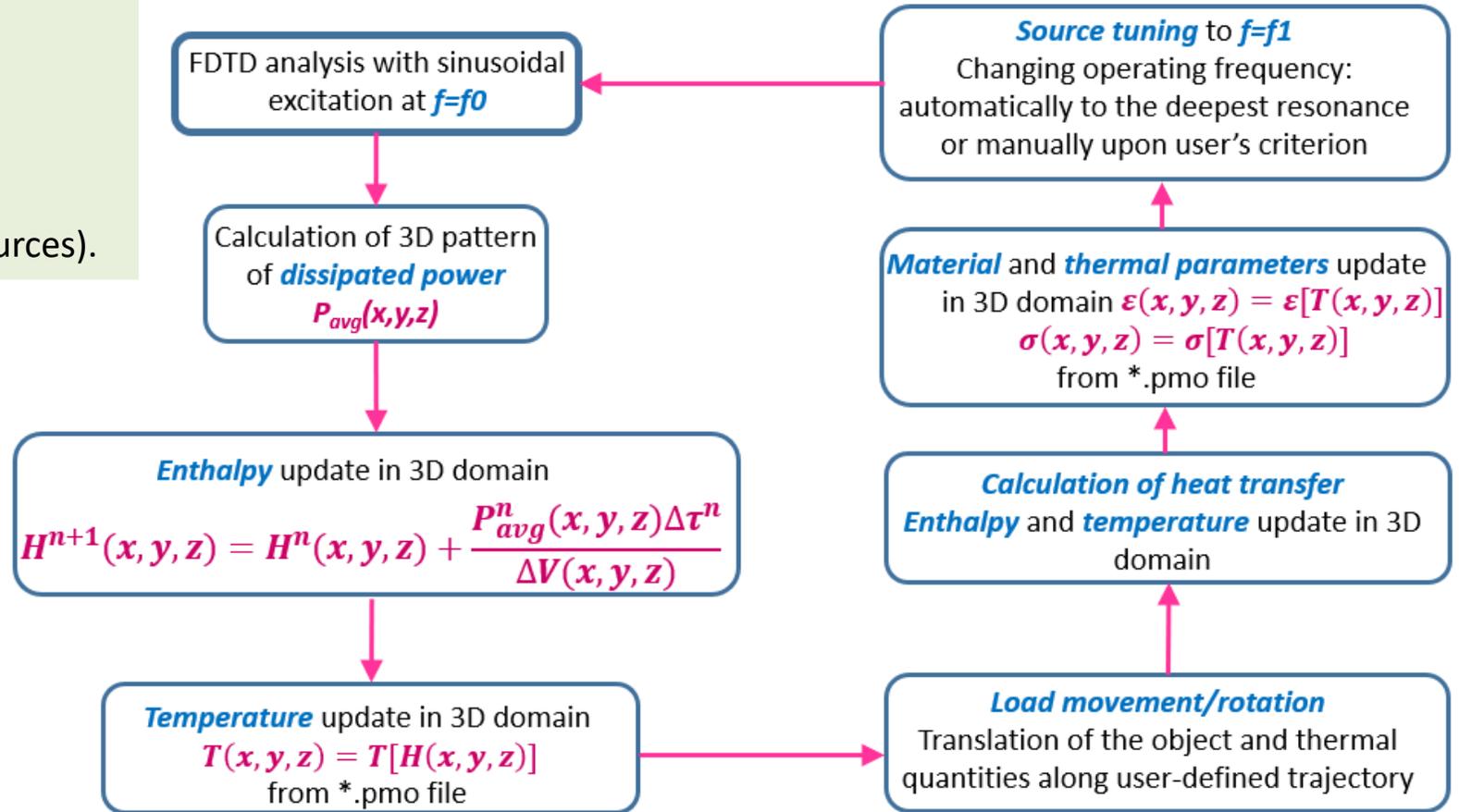
Industrial Design of Axisymmetrical Devices Using a Customized FDTD Solver from RF to Optical Frequency Bands

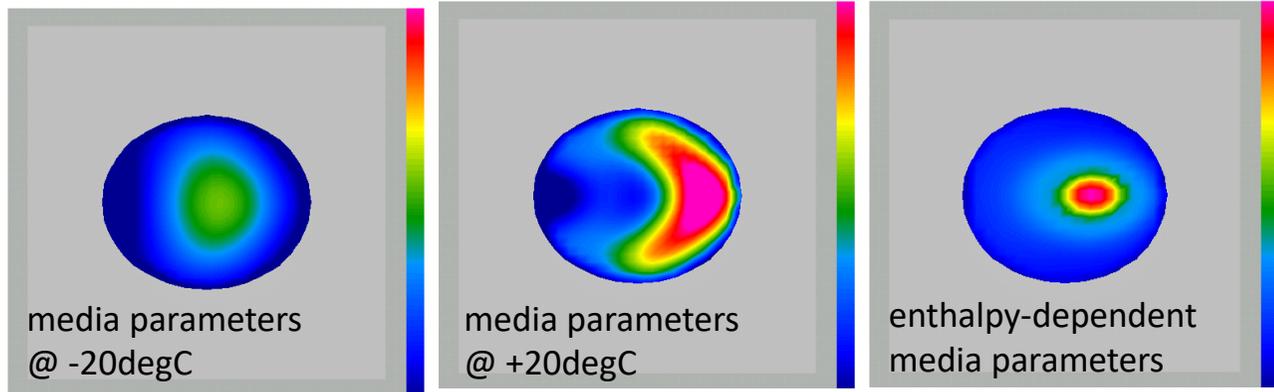
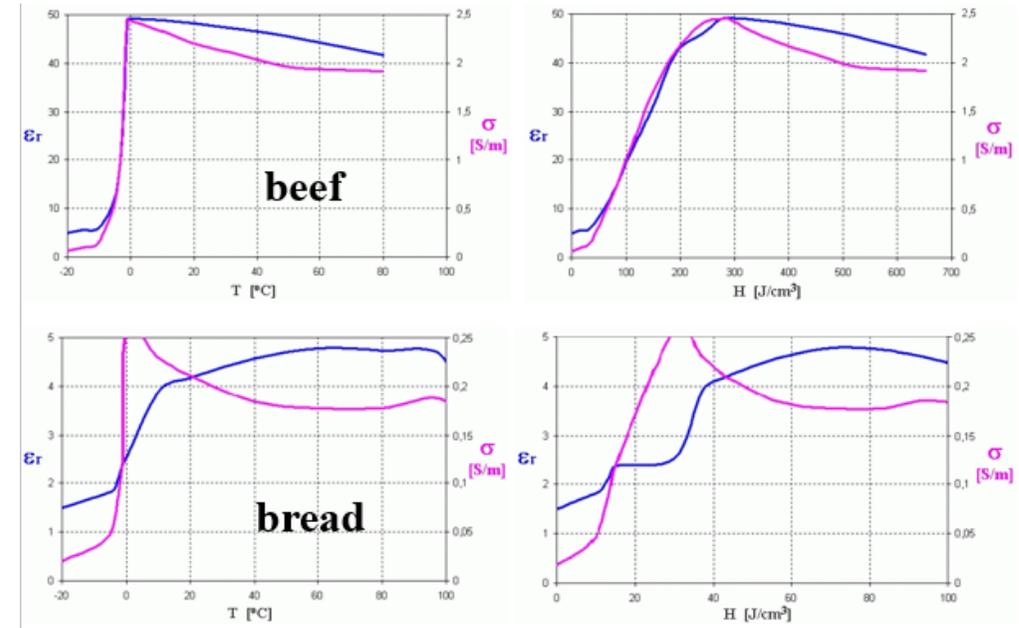
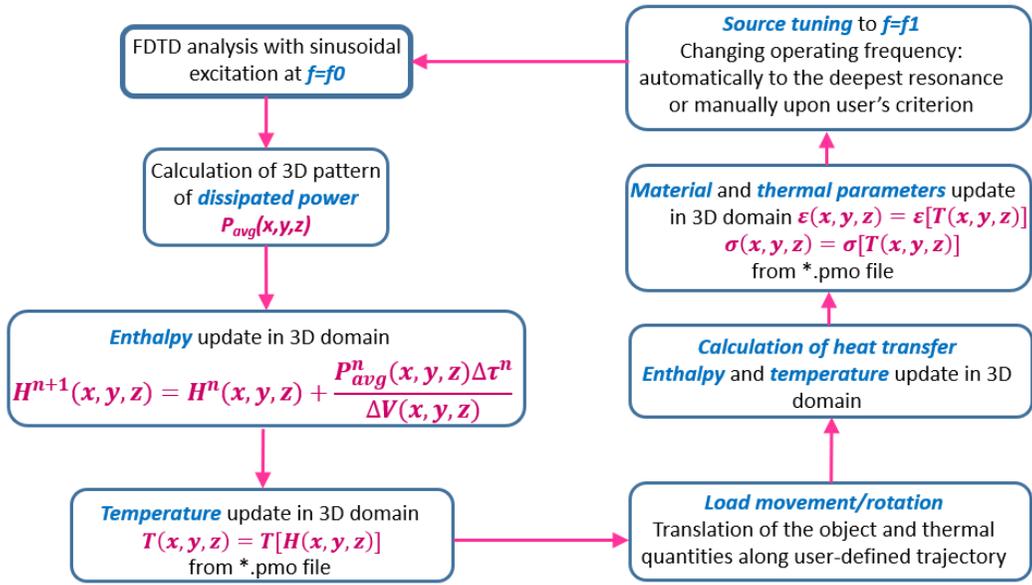
■ Malgorzata Celuch and Wojciech K. Gwarek

Bartłomiej Salski, Malgorzata Celuch, and Wojciech Gwarek

The time-domain approach allows us to dynamically and naturally modify during the heating:

- positions of objects,
- material parameters of heated objects,
- excitation (e.g. solid-state computer-controlled sources).

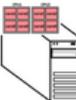




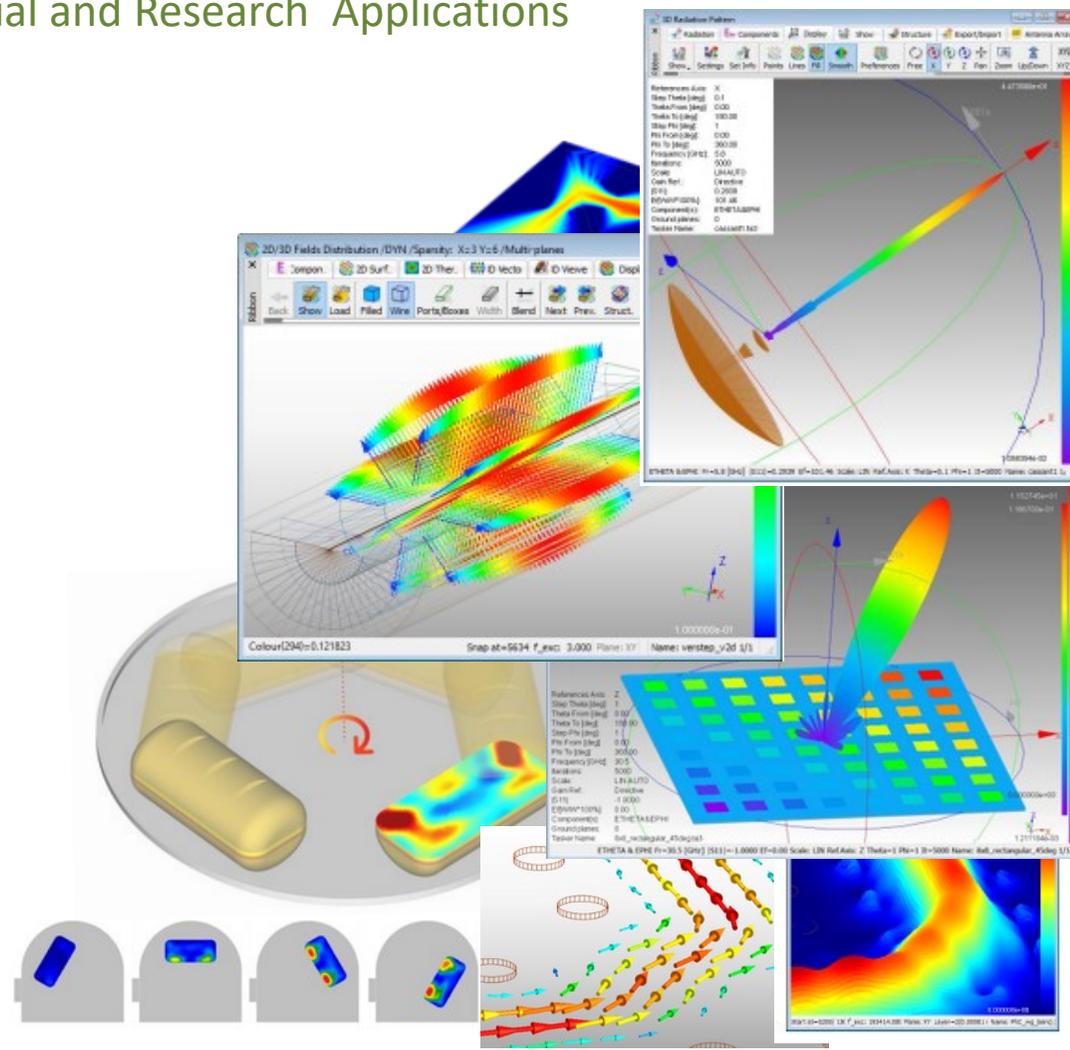
materials' data
courtesy P.O.Risman

Advanced Electromagnetic & Mutliphysics Simulation Software for Industrial and Research Applications

Key modules & functionalities:

- 
Full 3D EM solver with a range of unique models.
- 
Vector 2D (BoR), ultra fast solver applicable to the analysis of **axisymmetrical** devices. Almost instantaneous convergence!
- 
BHM Heat Module, heating analysis including loads rotation and translation, frequency tuning, **heat flow** and material parameters modification.
- 
QProny module for high Q-factor structures analysis.
- 
OptimiserPlus multiobjective optimiser which allows to finding an optimal solution in an automatic way.
- 
Multiprocessor/multicore and **MultiGPU** computing ensures **maximum** performance of your computer's resources


 QW-AddIn for Autodesk® Inventor® Software and more...

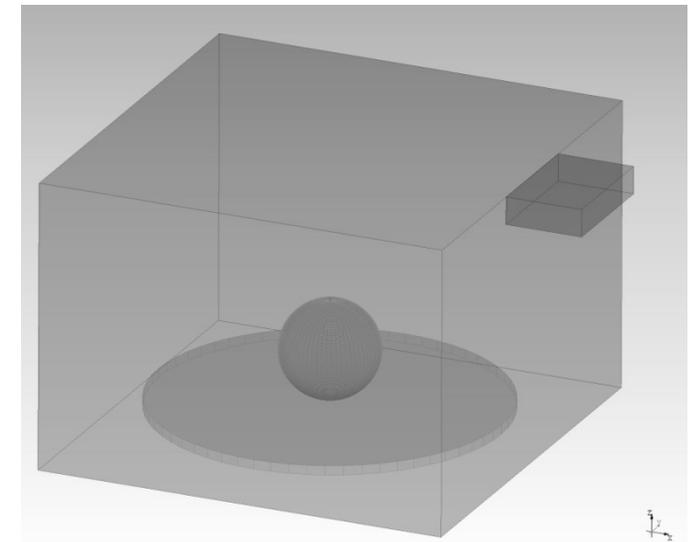
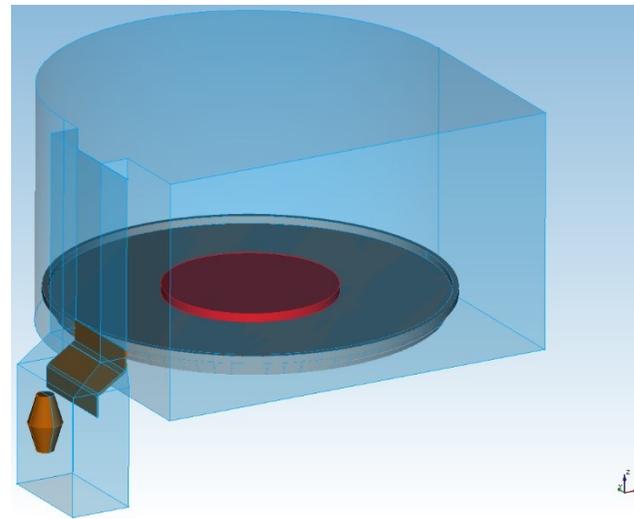




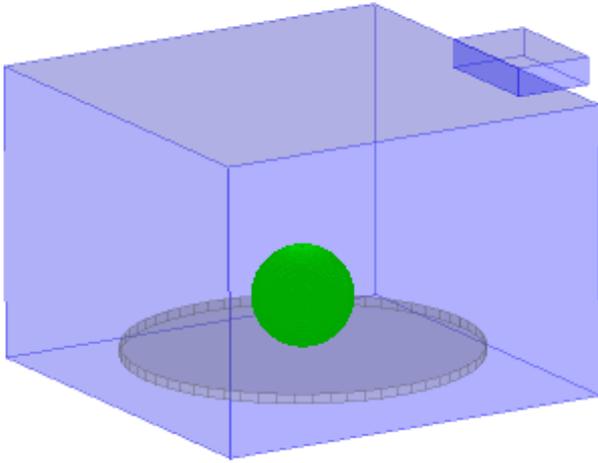
We focus on two modeling scenarios (“Elsevier MW Book” 2020):

1. a simple representative oven (Risman, Microwave World, 1998)
2. a complex commercial Whirlpool Max oven.

QWED team contributed 3 chapters.



[2]



QuickWave v2022 (FDTD)

Intel Core i7-8700 3.2 GHz, 6 Core(s)

RAM: 16 GB

Graphic Card: AMD Radeon Pro WX 3100

Microwave Oven Parameters

The oven has:

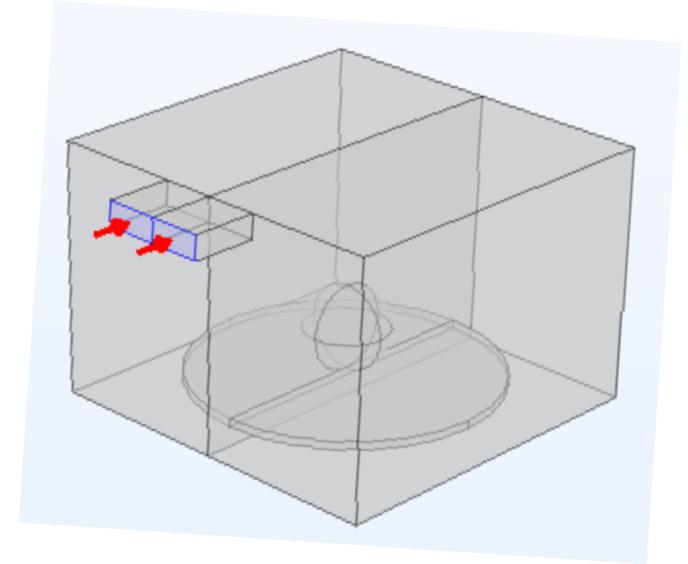
- a width of 267 mm,
- a depth of 270 mm,
- a height of 188 mm.

The waveguide's dimensions are:

- 50 mm in width,
- 78 mm in depth,
- and 18 mm in height.

The glass plate has:

- a radius of 113.5 mm,
- a height of 6 mm,
- and a base of 15 mm.



COMSOL Multiphysics 5.6 (FEM)

Intel i7-3820 CPU @ 3.6 GHz, 4 Core(s)

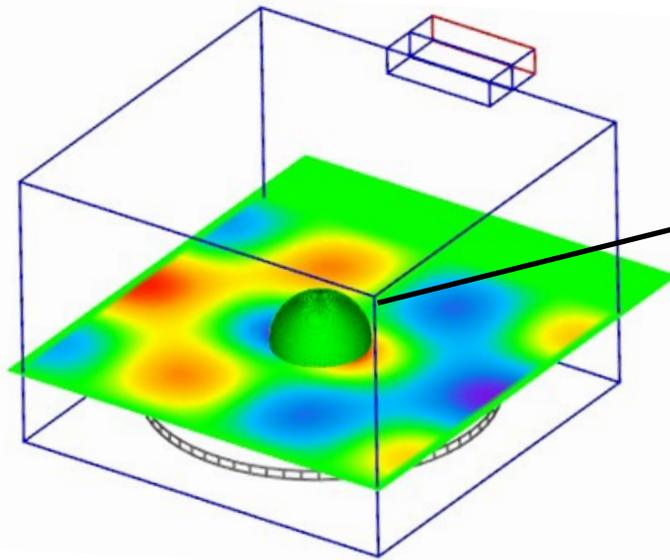
RAM: 64 GB

Graphic Card: NVIDIA GeForce GTX 660 Ti

The potato has a radius of 31.5 mm and its initial temperature is **8°C**.

Relative permittivity of potato is equal to **65** and its conductivity to **2.722 S/m**.

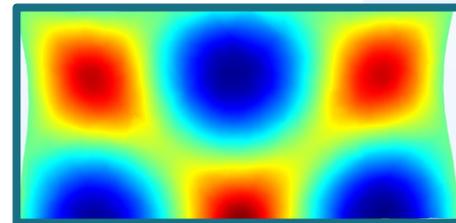
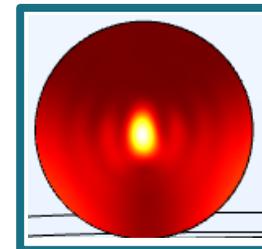
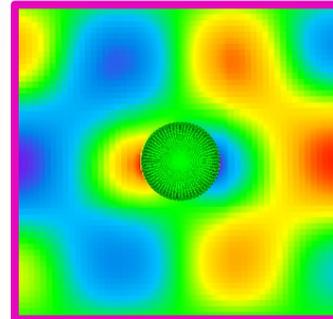
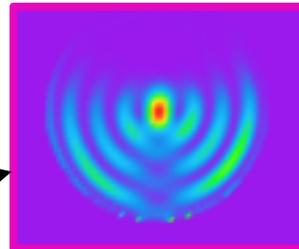
A Simple Benchmark (2)



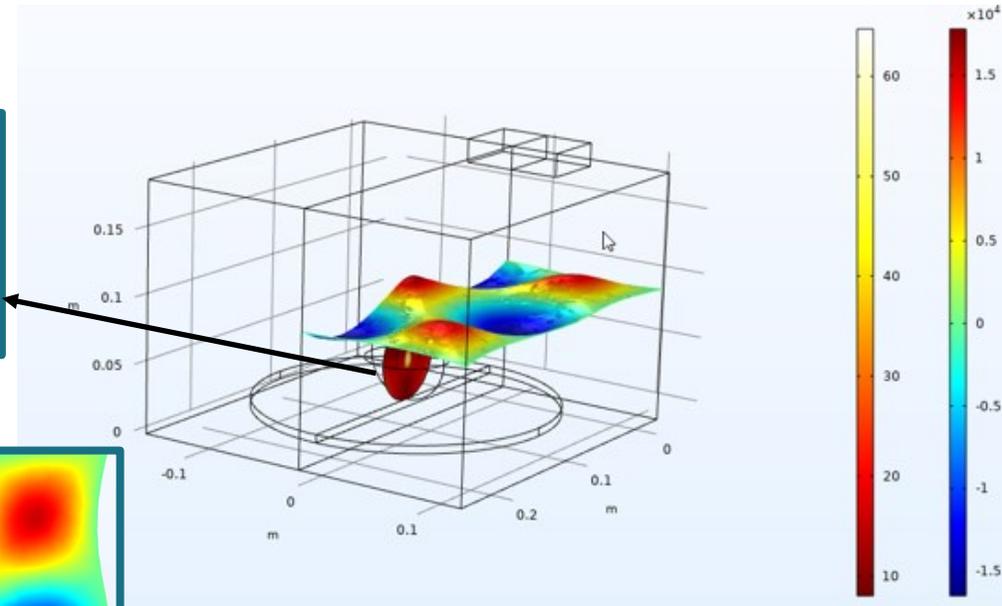
QuickWave v2022 (FDTD)

Simulation time: 00:00:42 (h:min:sec)

Temperature distribution



Electric field distribution



COMSOL Multiphysics 5.6 (FEM)

Simulation time: 00:01:05 (h:min:sec)

Simulation info

For both methods, a Frequency step of **0.001 GHz** was chosen.

COMSOL Multiphysics 5.6 (FEM)

Simulation time: 01:04:12 (h:min:sec)

RAM: 4220 MB

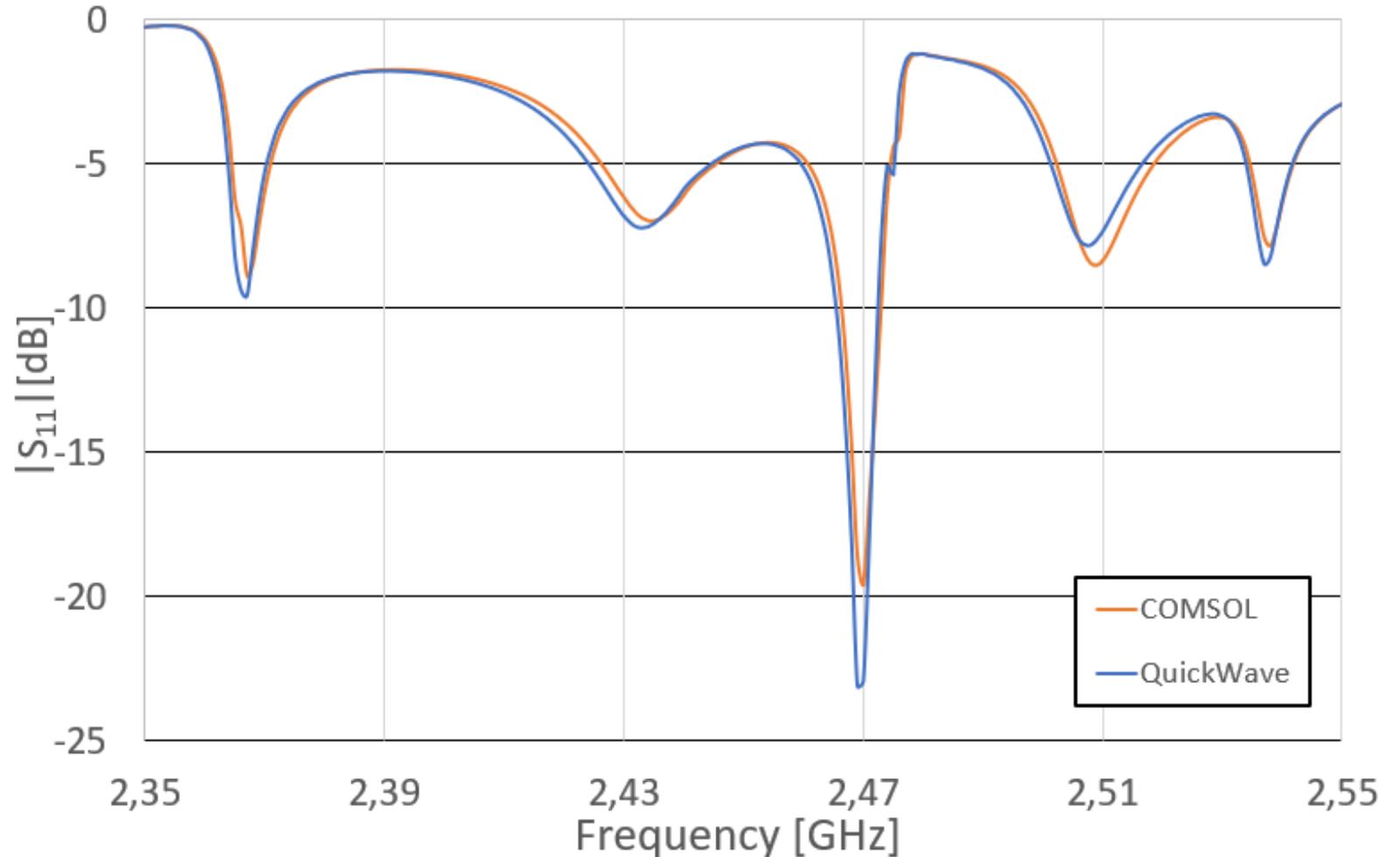
Cells: 60 004

QuickWave v2022 (FDTD)

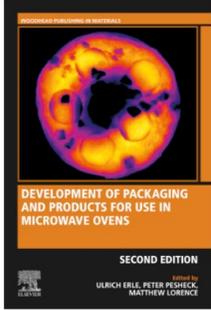
Simulation time: 00:05:03 (h:min:sec)

RAM: 364 MB

Cells: 3 614 128

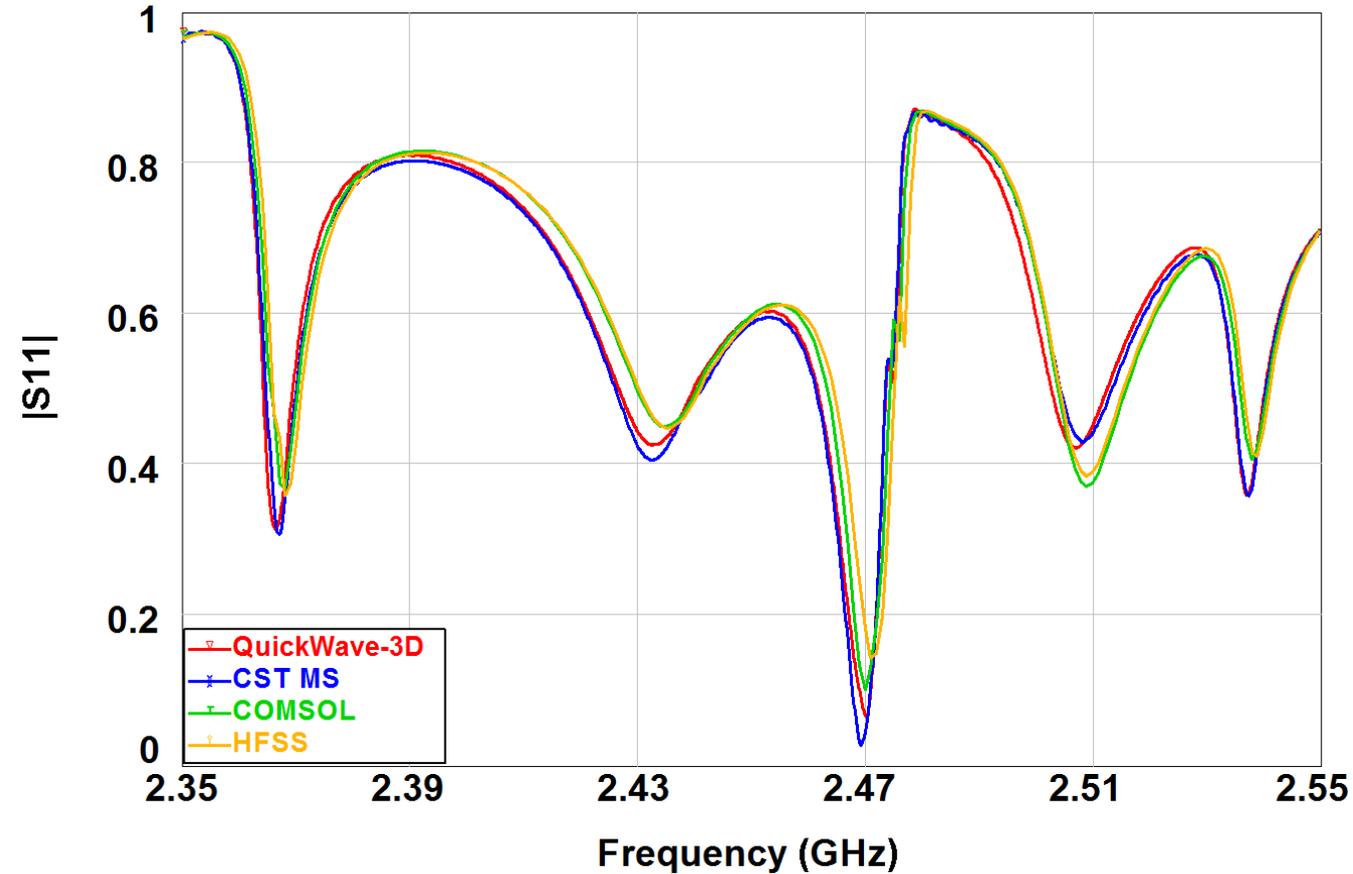


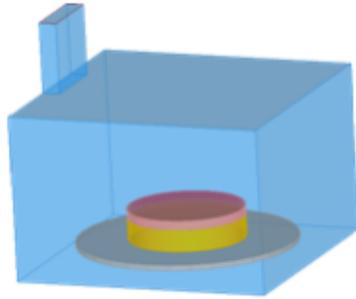
A Simple Benchmark (4)



	Computation time ^a	Element/cell count	RAM usage
QuickWave-3D	3 min 43 s	3 602 463	217 MB (GPU memory for scenario) 288 MB (RAM for exe)
CST MS	5 min 44 s	4 591 720	2194 MB (peak memory reported in log)
COMSOL	25 min 20 s	60 004	3300 MB
ANSYS HFSS v19.2	43 min 53 s	24 014	2168 MB

^a The calculations were performed with the most optimum acceleration regime available for each software licence. For FDTD based software, GPU acceleration (on Nvidia GeForce GTX Titan for QuickWave-3D and Tesla K40c for CST MS) was adopted, and for FEM based solvers, multicore computations (on AMD Ryzen 7 1800x and Intel i7-3930K processors for COMSOL and ANSYS HFSS, respectively) were performed.

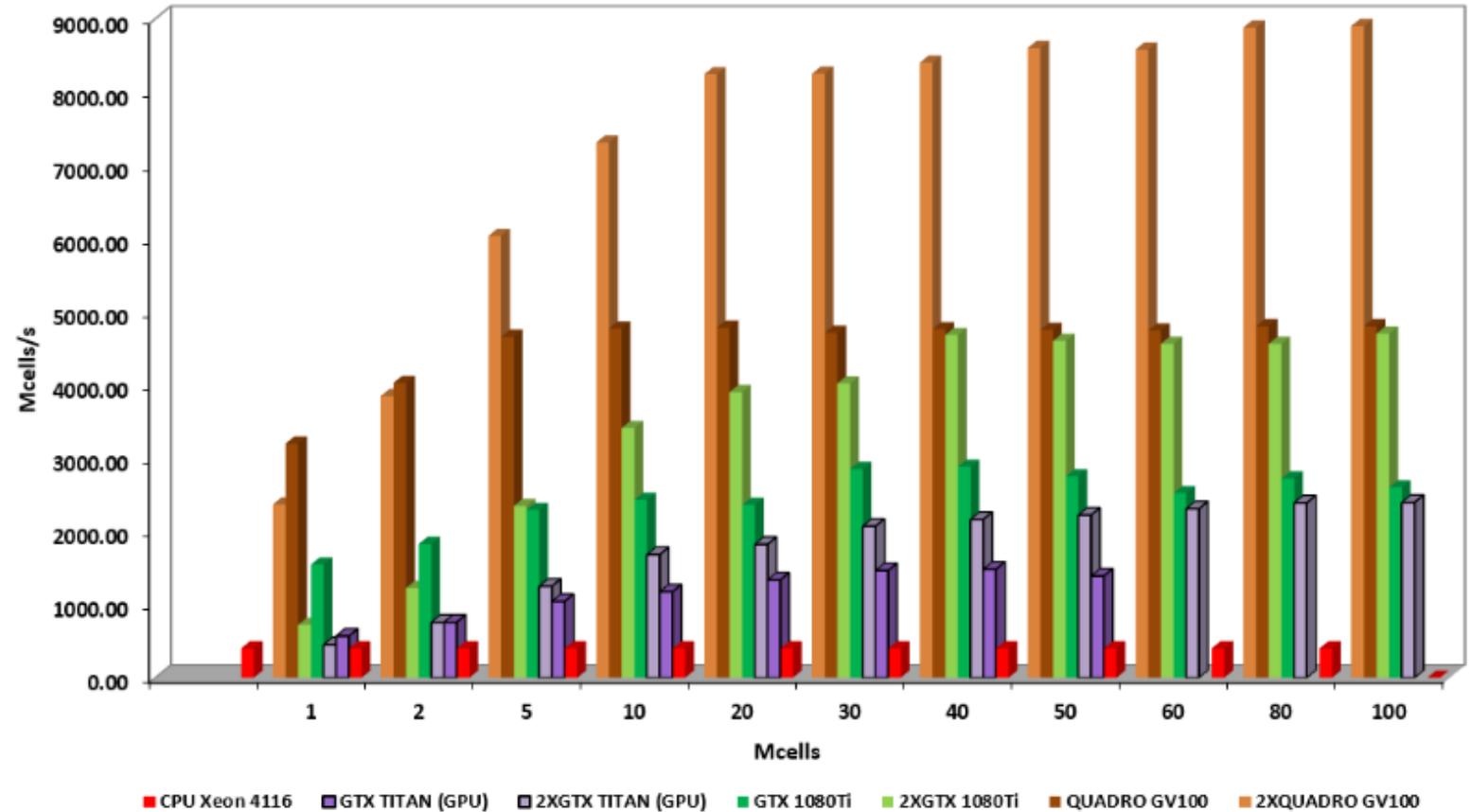




Popular hardware acceleration options include:

1. moving from CPU to GPU
2. dividing the computation region into subregions, simulated on separate processors.

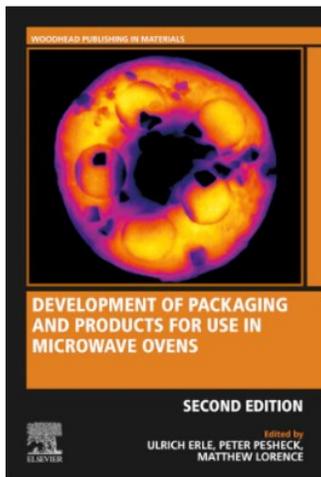
A combination of both options – **MultiGPU** – is especially powerful.



SpeedUp of the GPU and MultiGPU simulation scenario (project divided along Y direction into two symmetrical subregions) computation of a beefburger placed in a cavity oven (3D example) compared to QW-OMP version on Xeon 4116.

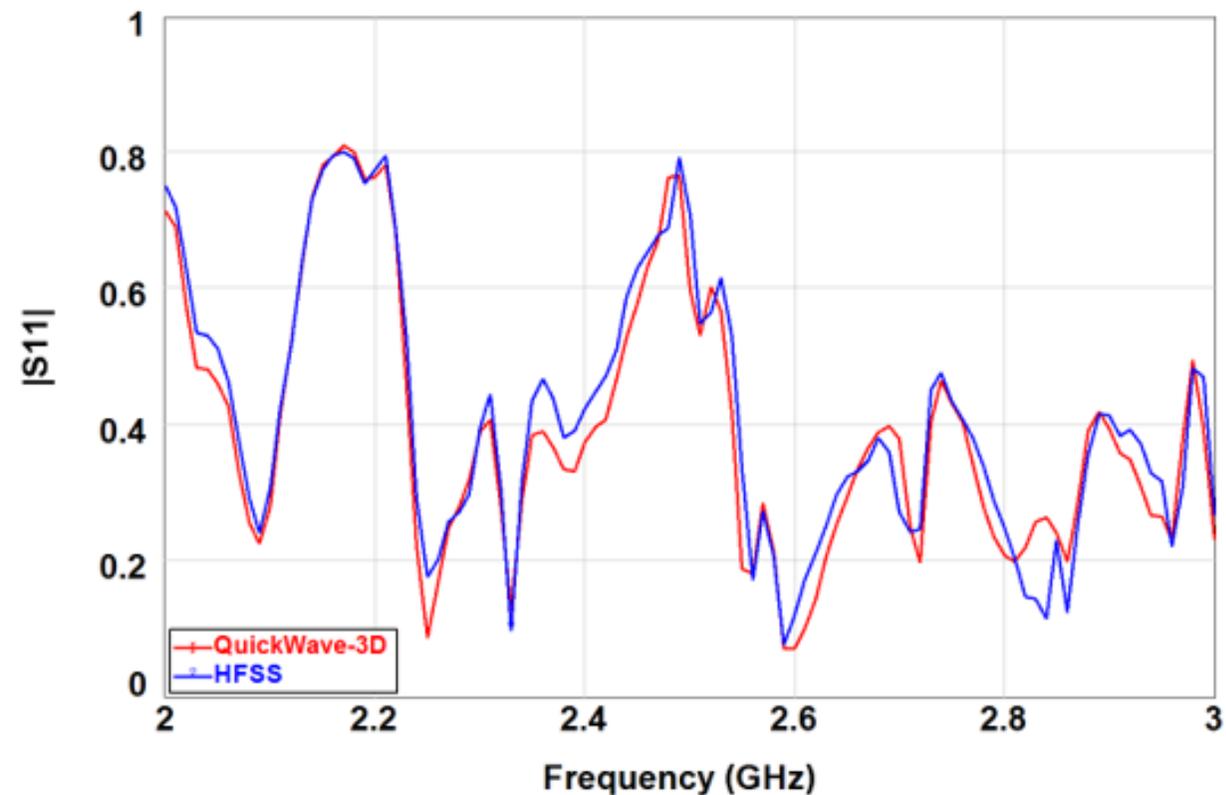
Quadro GV100 cards have been provided by Servodata Elektronik Sp. z o.o., Poland

Max Oven - EM Model (1)



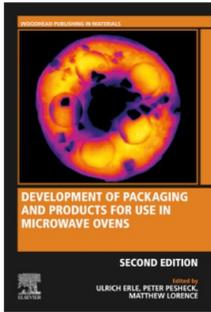
	Computation time ^a	Element/cell count	RAM usage
QuickWave-3D v2018	1 min 18s	1 422 900	86 MB (GPU memory for scenario)
ANSYS HFSS v19.2	29 min 3s	35 407	319 MB (RAM for exe)
QuickWave v7.0	39 min 17s	1 323 120	2844 MB (peak memory reported in log)
HFSS v11	300 min 8s	31 000	136 MB
			955 MB

^a The calculations were performed with the most optimum acceleration regime available for each software licence. For FDTD based software GPU acceleration (on Nvidia GeForce GTX Titan) was adopted, and for FEM based solvers, multicore computations (on Intel i7-3930K processor) were performed. For QuickWave v7.0 and HFSS v11, calculations were performed on 2.21 GHz AMD Athlon 3500+ and 2.4 GHz Intel Pentium IV platform respectively.



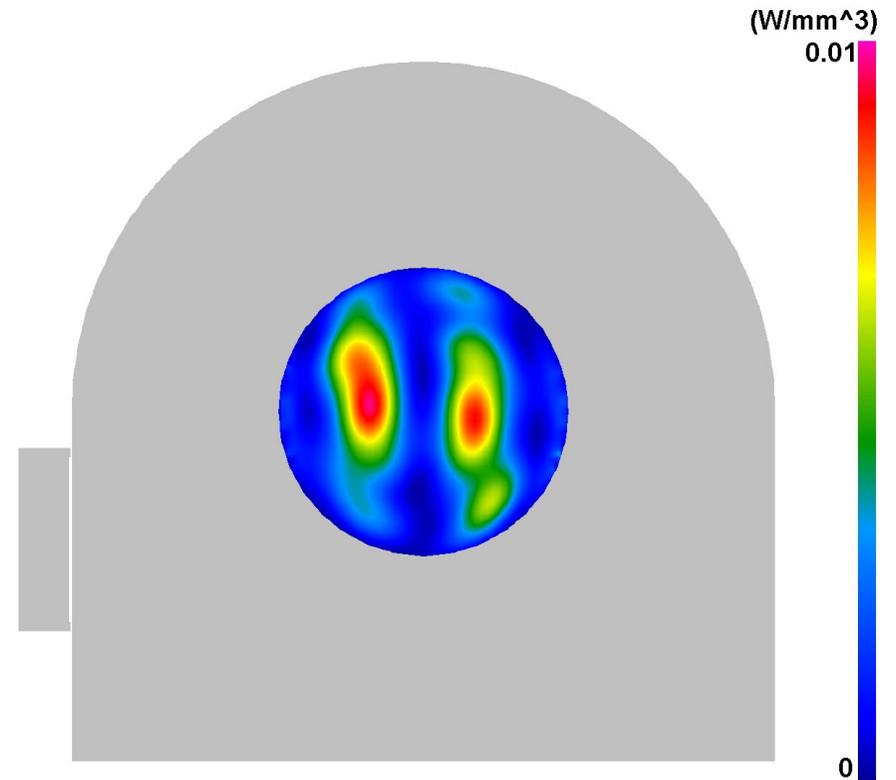
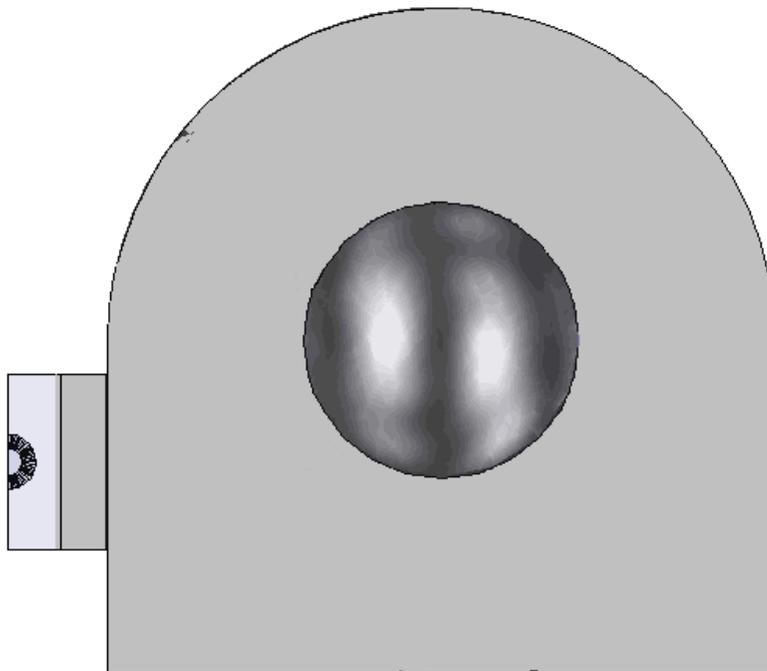
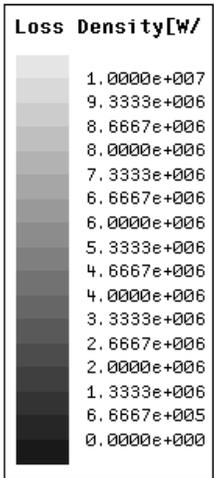
Max Oven – EM Model (2)

Dissipated power density distribution in the cross-section of the load heated from in Whirlpool Max.

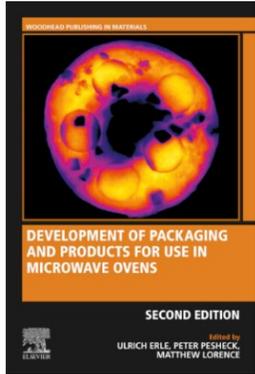


HFSS package v11 (values given in W/m³)

QuickWave-3D v2018 package (values given in W/mm³)

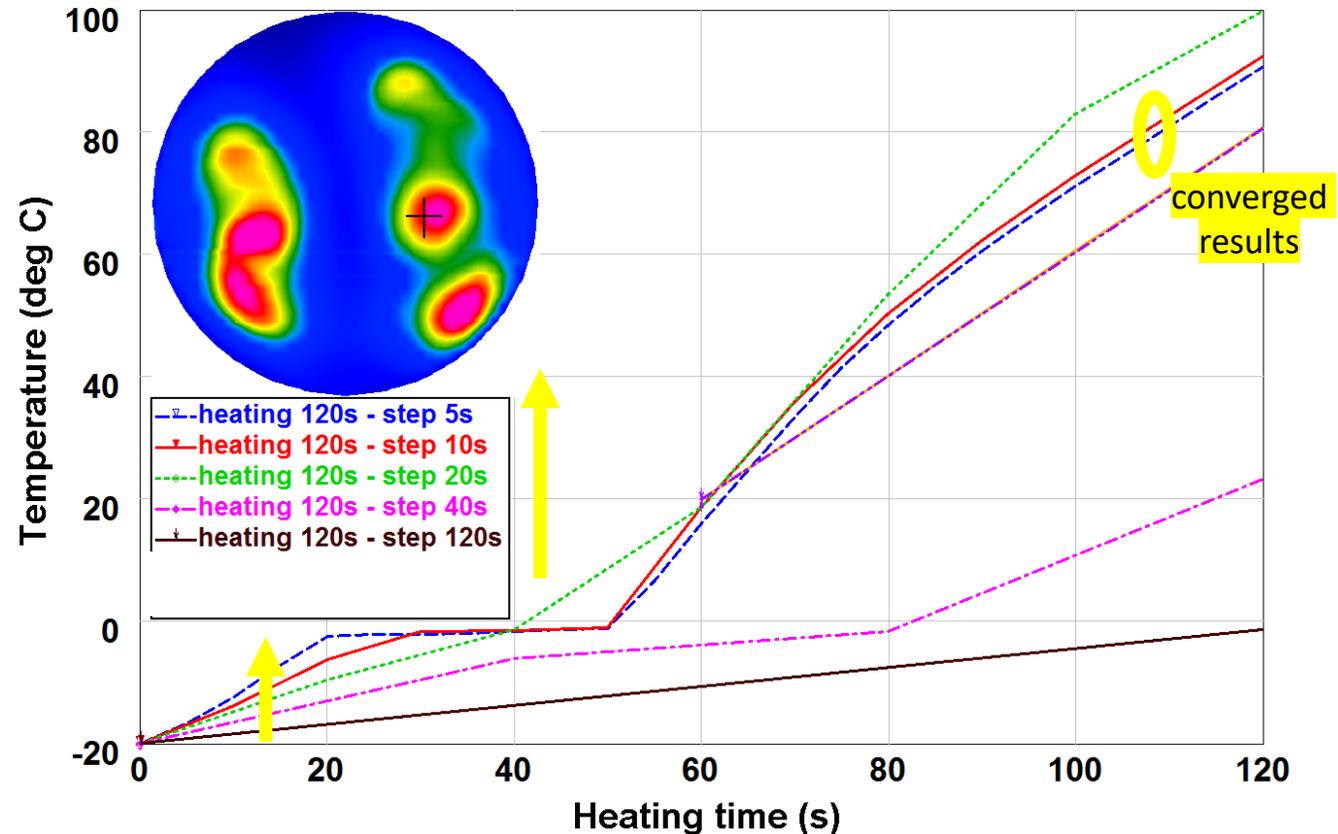
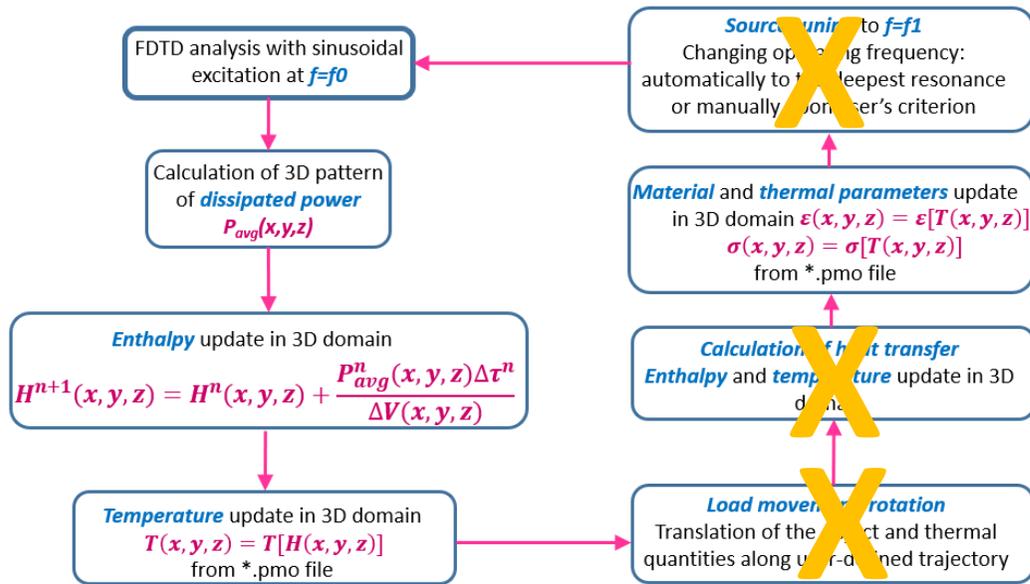


Max Oven – Multiphysics Model (1)

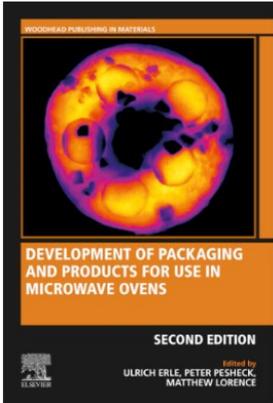


Thermally dependent load parameters – effect of parameterisation of the nonlinear heating process

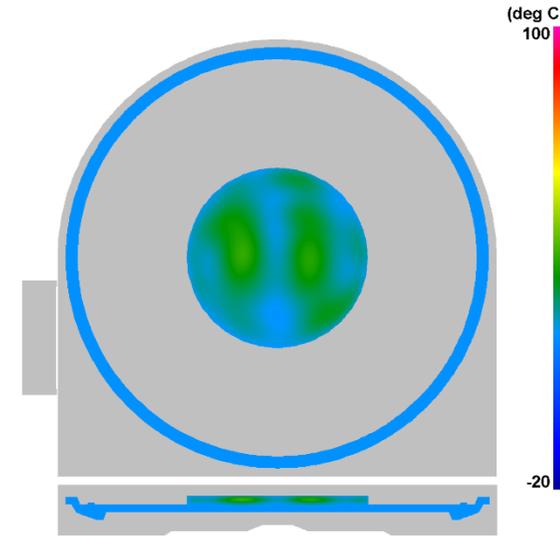
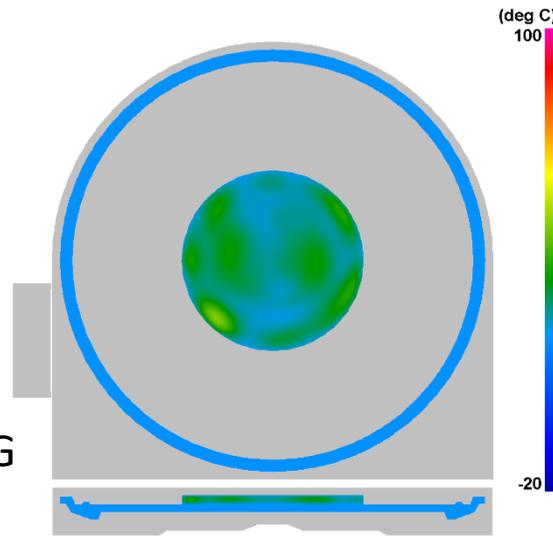
- same total heating time
- increased number of “thermal” computational iterations, at which material parameters are automatically updated based on current temperature reached in a given FDTD cell



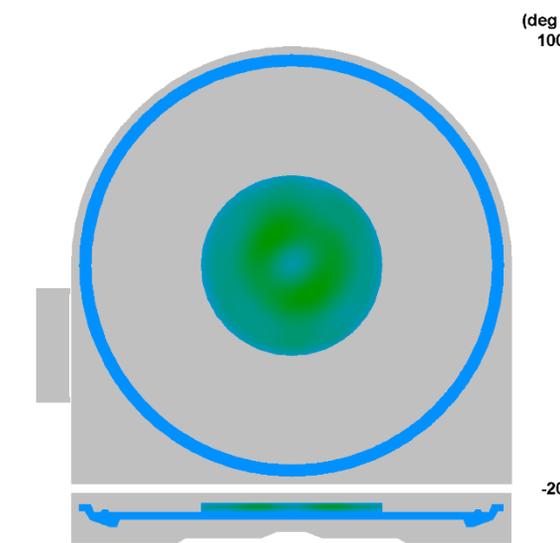
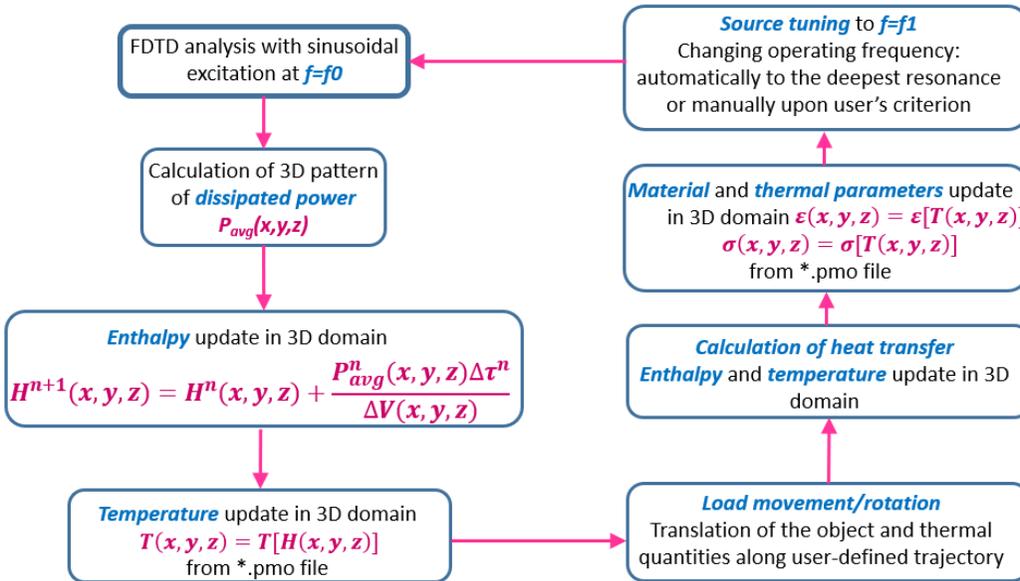
Max Oven – Multiphysics Model (2)



HEAT FLOW +
MAGNETRON PULLING



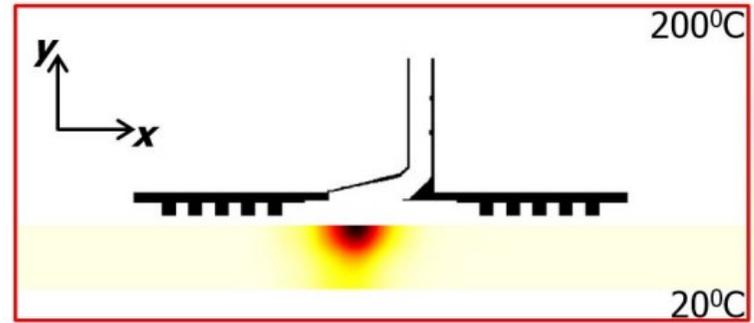
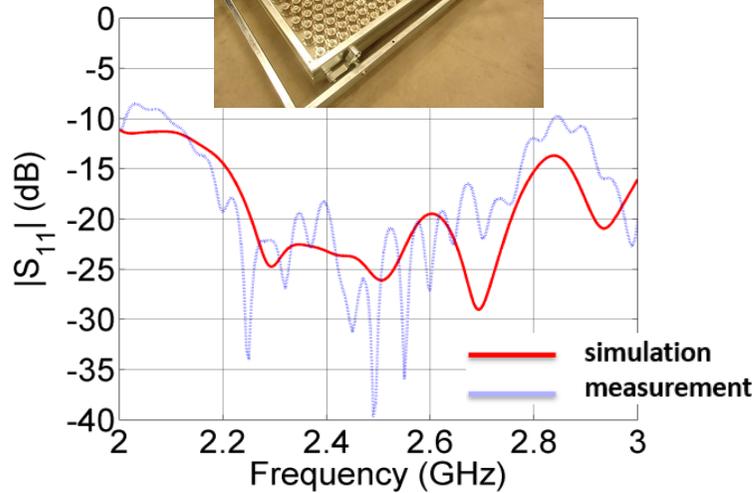
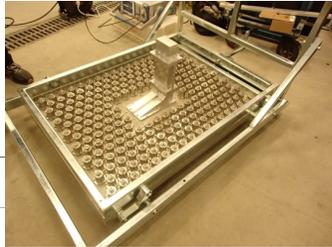
HEAT FLOW



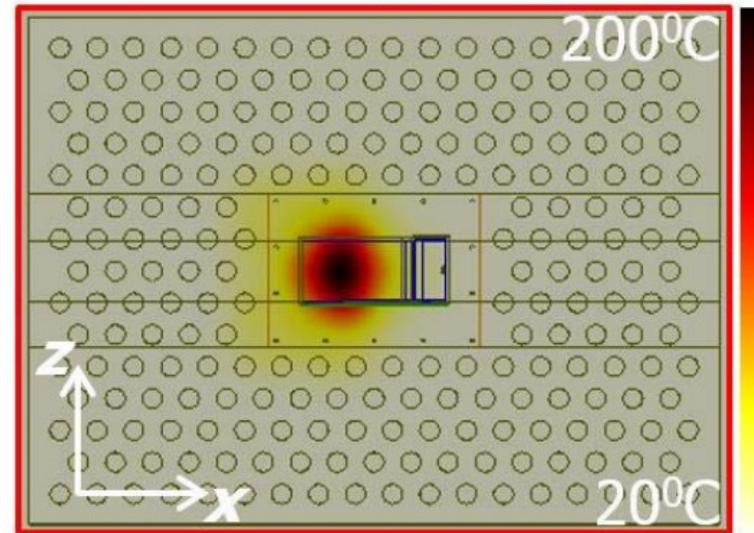
HEAT FLOW +
LOAD ROTATION

Note on “Real” Problem Size

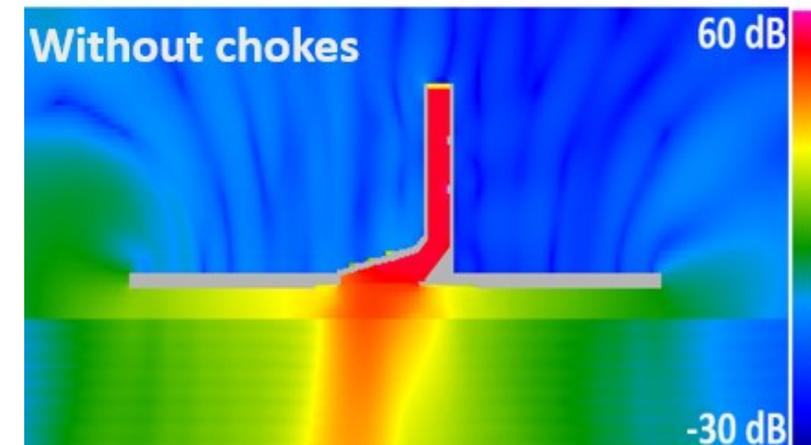
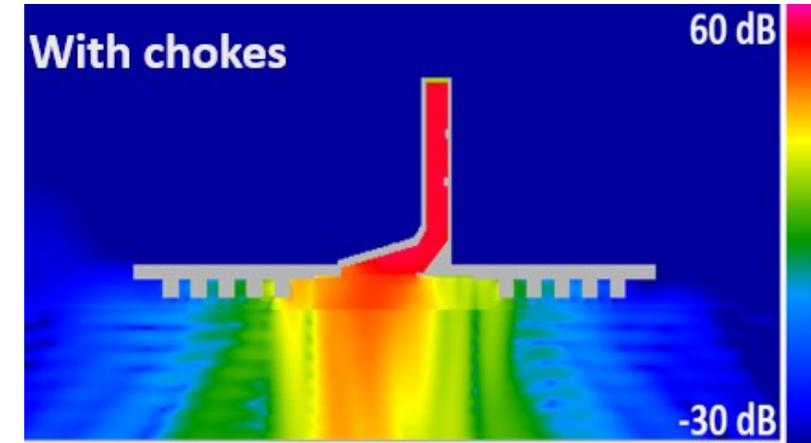
Example: applicator for heating bituminous surfaces (with a safety system including chokes to block leakage)



(a)



(b)



FDTD cell size $\geq 1.3\text{mm}$
Problem size: several wavelengths

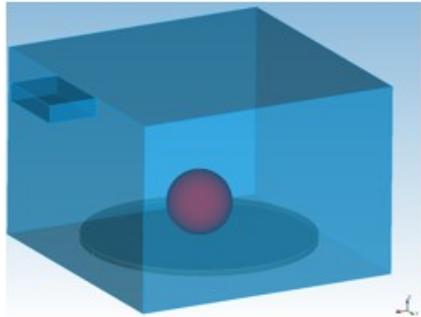
FDTD model of 9.4 million cells
RAM: 779 MB

Simulation time: 26 seconds

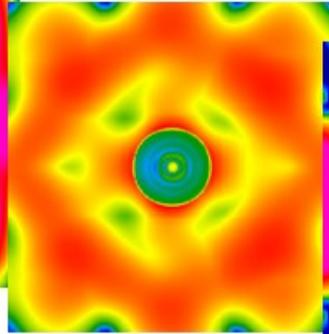
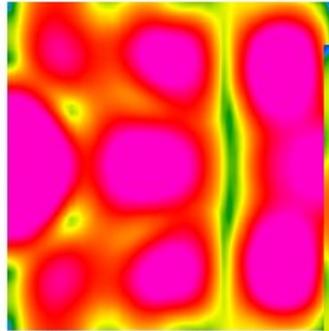
FDTD is particularly advantageous for problems “big” wrt to wavelength, which are too big for running FEM simulations on available computers

NEW: New-Field Imaging Function

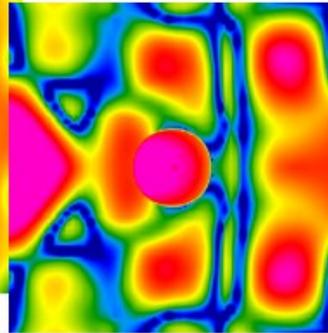
Separation of incident and diffracted fields for biomedical research applications (*request of P.O.Risman, Malardalen Univesity*)



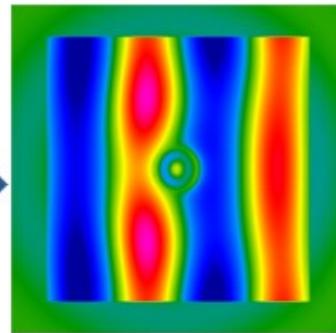
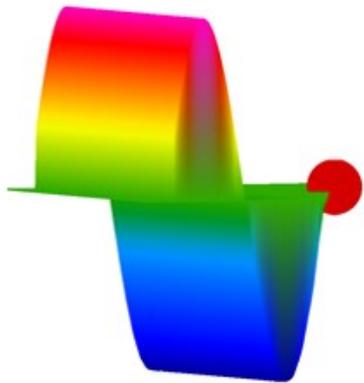
E-field in an empty cavity



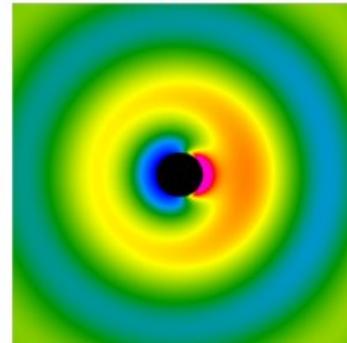
E-field in a loaded cavity



Scattered near-field in cavity

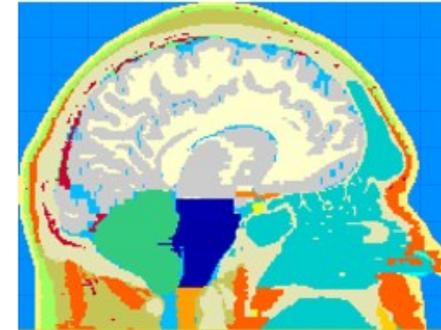


Total field
Focusing by the load
„exploding egg effect”

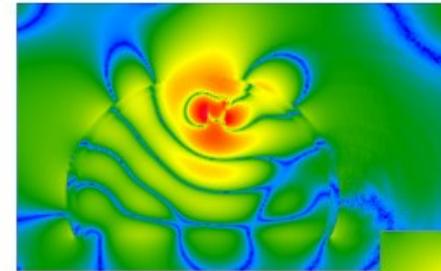


Diffracted field reveals
cause of focusing:
circumferential resonance

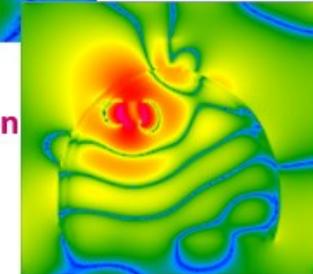
Detection of inhomogeneities in tissues



AustinMan model* converted to **QuickWave EM** software for Mälardalen University, Sweden



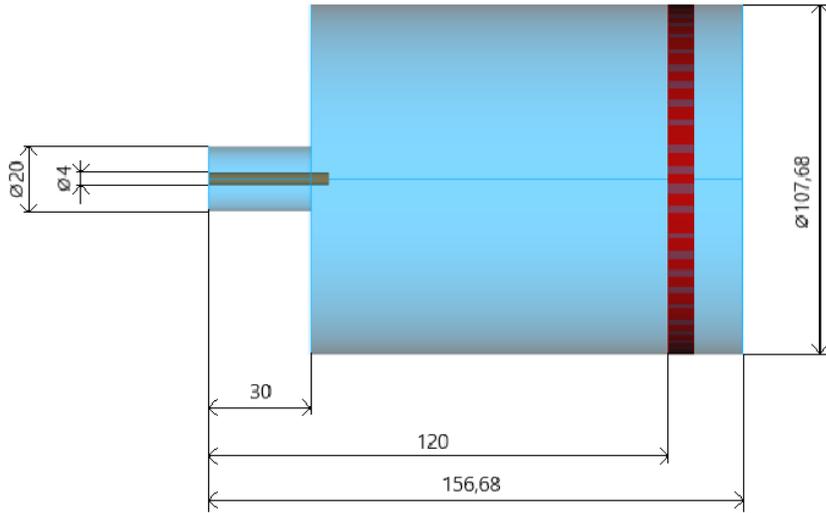
- ✓ Tumours & haemorrhages detection
- ✓ Optimisation of multi-antenna tomographic systems



26

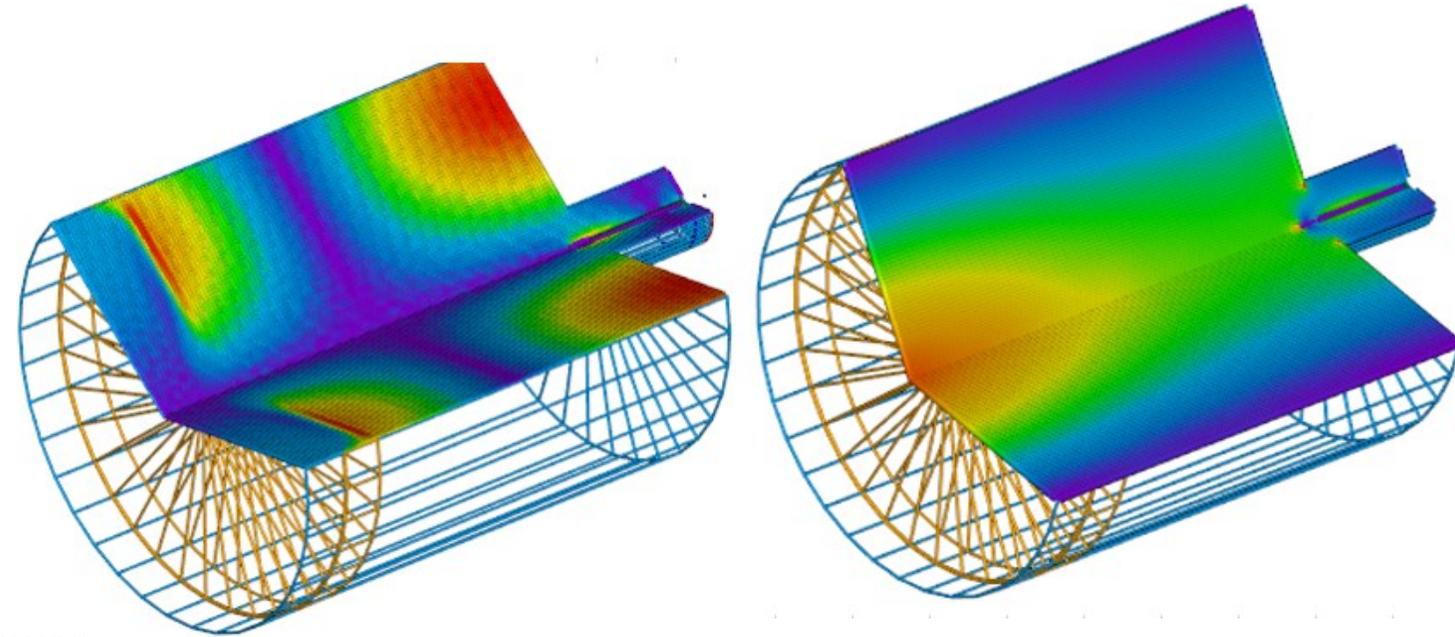
* <https://sites.utexas.edu/austinmanaustinwomanmodels/>

Multiphysics Modeling of BoR Scenarios (1)



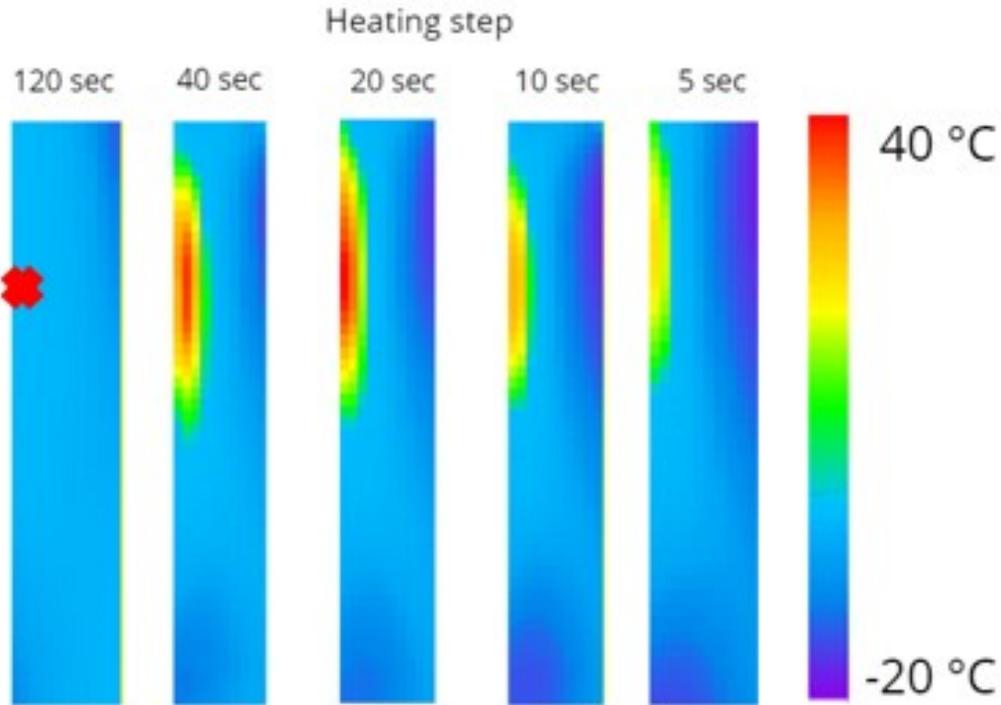
Microwave Applicator dimensions [3]

- The TE_{110} mode cannot exist in the resonator; the lower mode of the TE family is TE_{111} , and its eigenfrequency depends on the length of the resonator.
- Microwave heating applicators that support TM modes can use both electric field components - normal and tangential to a flat load placed in parallel to the resonator's bottom and cover.

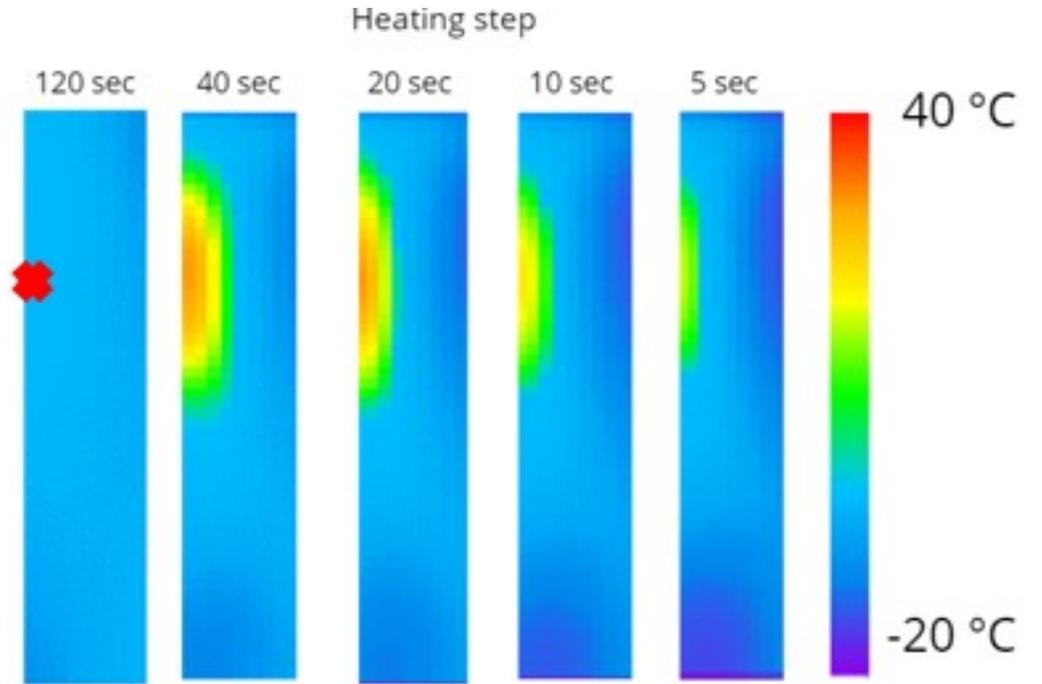


Distribution of the angular magnetic field and electric field of the TM_{011} mode, in a 270 degree view of the cylinder.

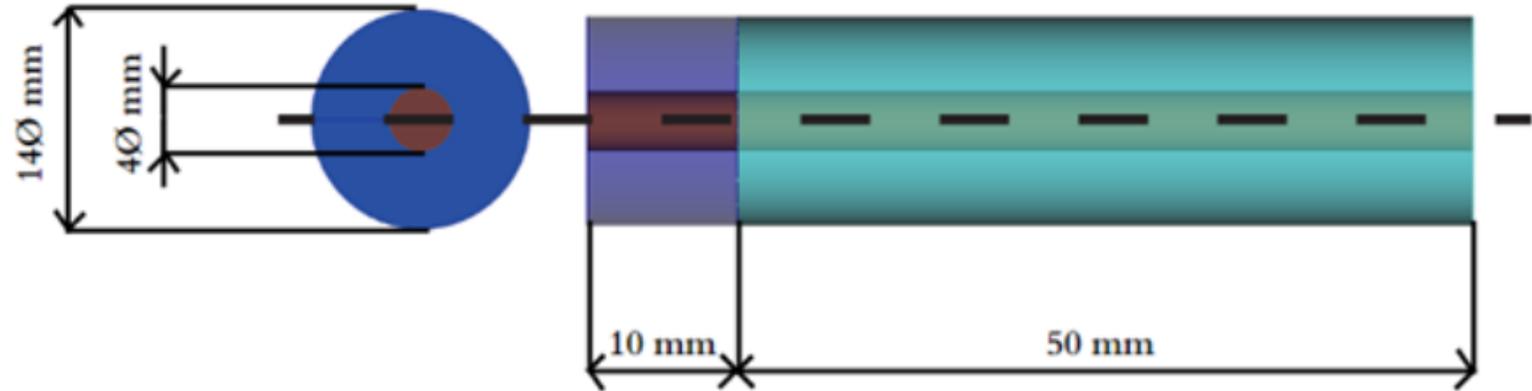
- Beef case



Distribution of final temperature in beef after heating for 120 seconds (**heat flow neglected**) - parameterised simulations using different heating steps.



Distribution of final temperature in beef after heating for 120 seconds, **including heat flow** phenomenon – parameterised simulations using different heating steps.



The battery being considered has a collector at its center, which acts as a perfect electric conductor (PEC) in the simulation. At the starting point of the system lies a source that is excited at a sinusoidal frequency of **1 or 10 GHz**. A 10 mm air separator is also present, with its reference plane situated in the middle. Following this is the electrolyte, which is a lossy material that terminates with a special symmetrical boundary condition of magnetic type design known as a perfect magnetic conductor (PMC).

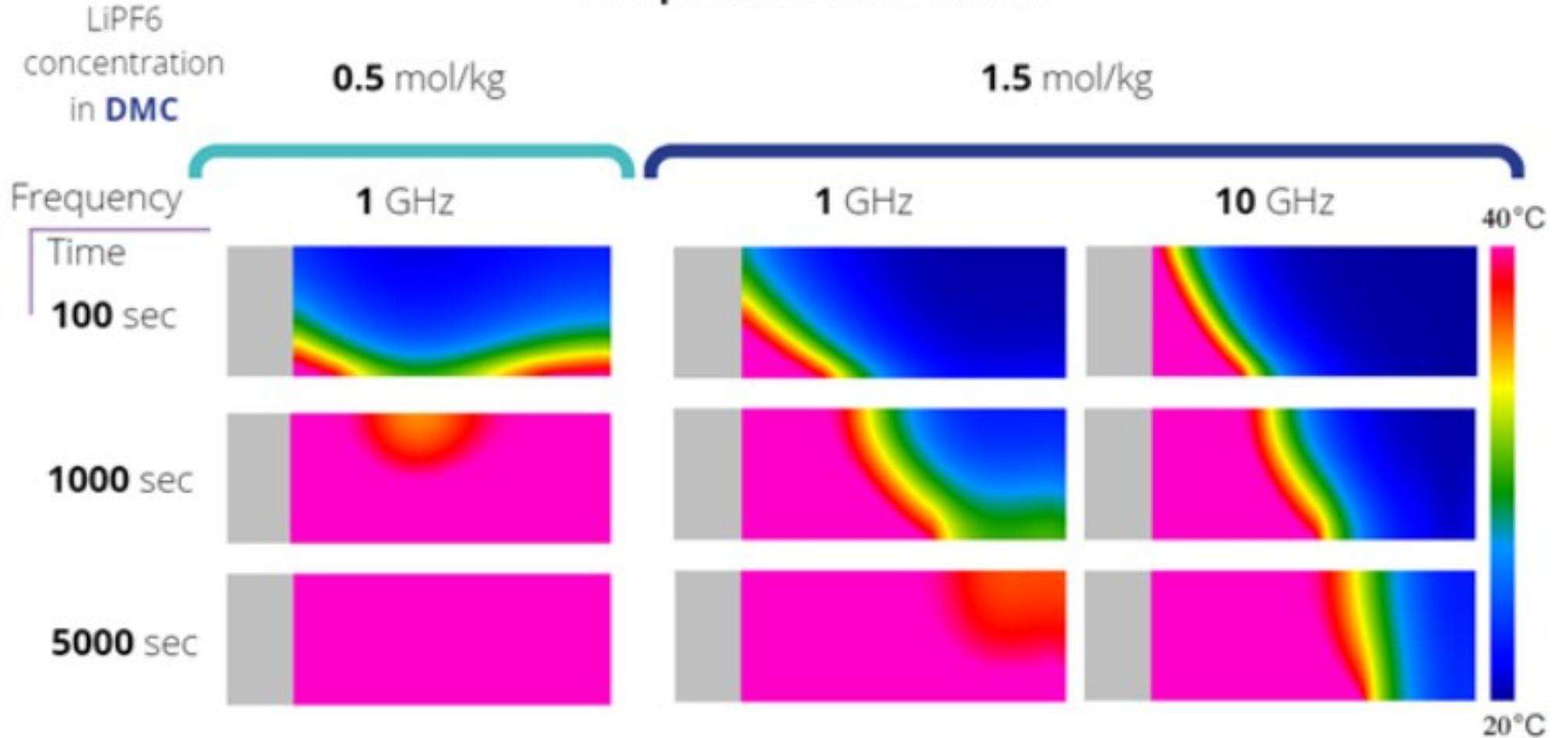
Temperature [°C]	LiPF6 concentration* [mol/kg]		Specific Heat capacity** [J/g°C]	Density* [g/cm ³]	Dielectric Constant* [F/m]
	0.5	1.5			
	Conductivity* [S/m]				
0	0.2	0.58	1.704	1.063	3.1075
10		0.65			
20		0.82			
30		1.04			
40		1.52			

*E. R. Logan et al 2018 *J. Electrochem. Soc.* **165** A705

** Zhou, Y., Wu, J. and Lemmon, E. (2011), Thermodynamic Properties of Dimethyl Carbonate, *J. Phys. & Chem. Ref. Data (JPCRD)*, National Institute of Standards and Technology, Gaithersburg

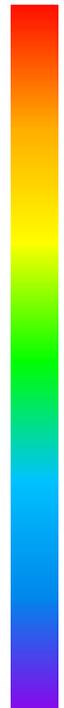


Temperature distribution



- Beef case

80 °C

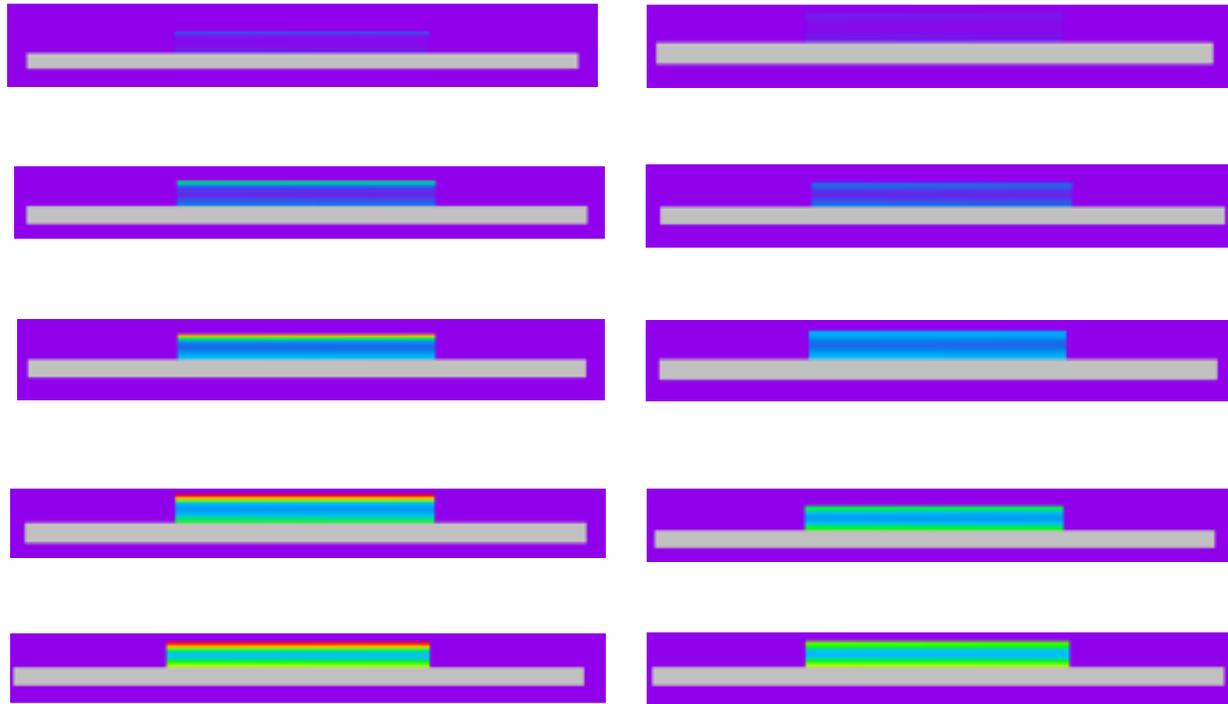


20 °C

Heat Flow with radiation

Heat Flow without radiation

Heating Time



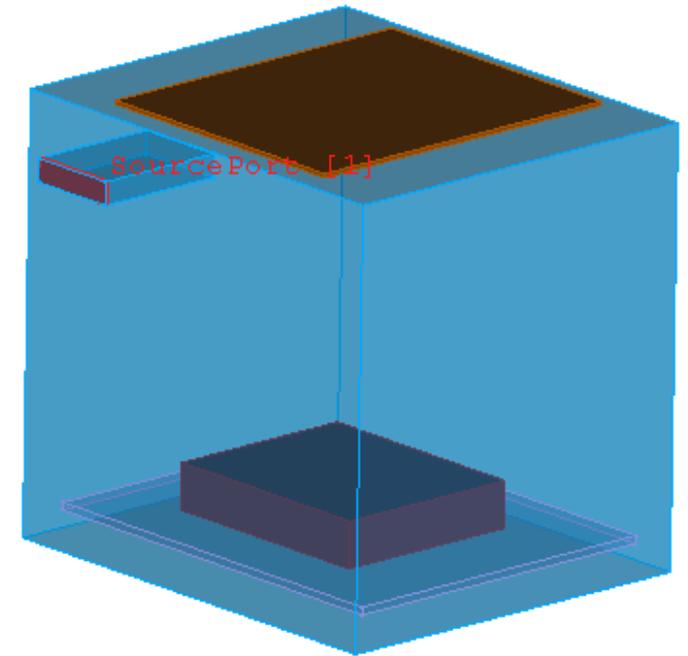
1 second

5 seconds

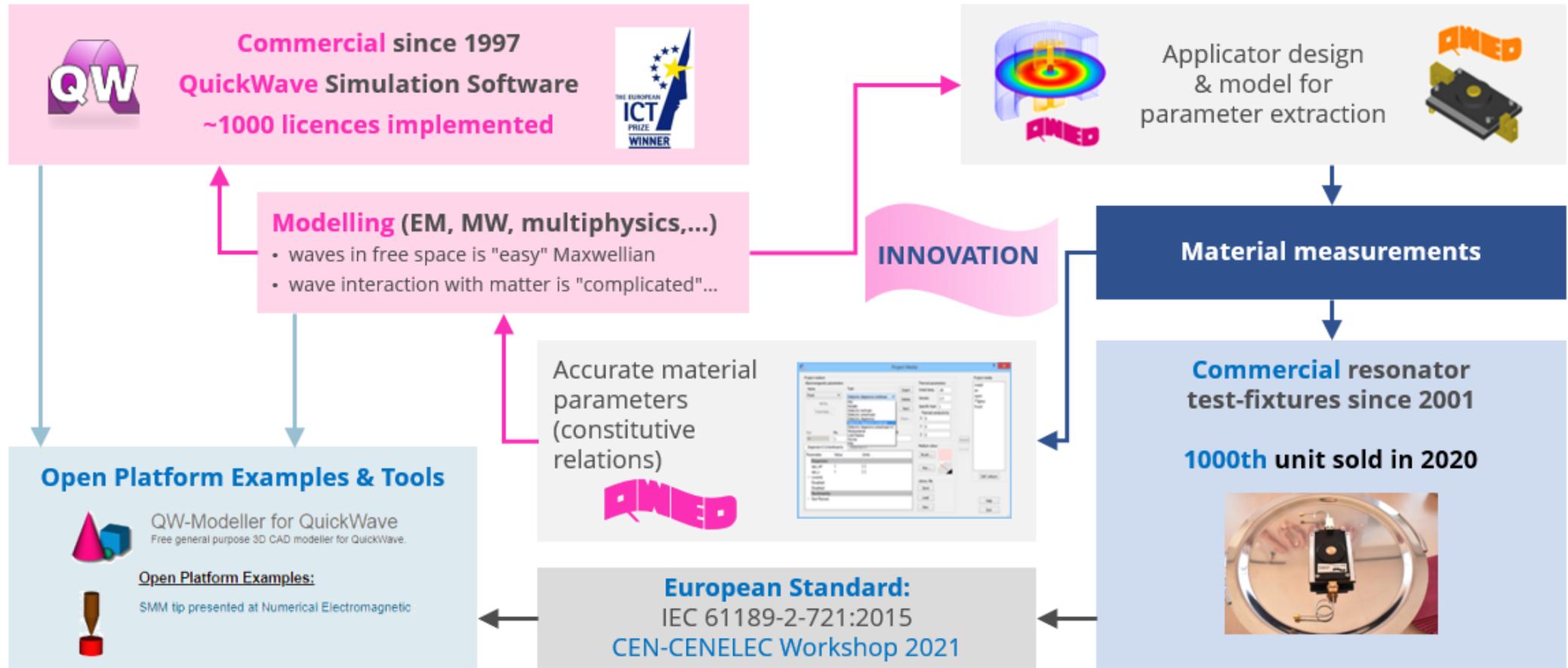
10 seconds

15 seconds

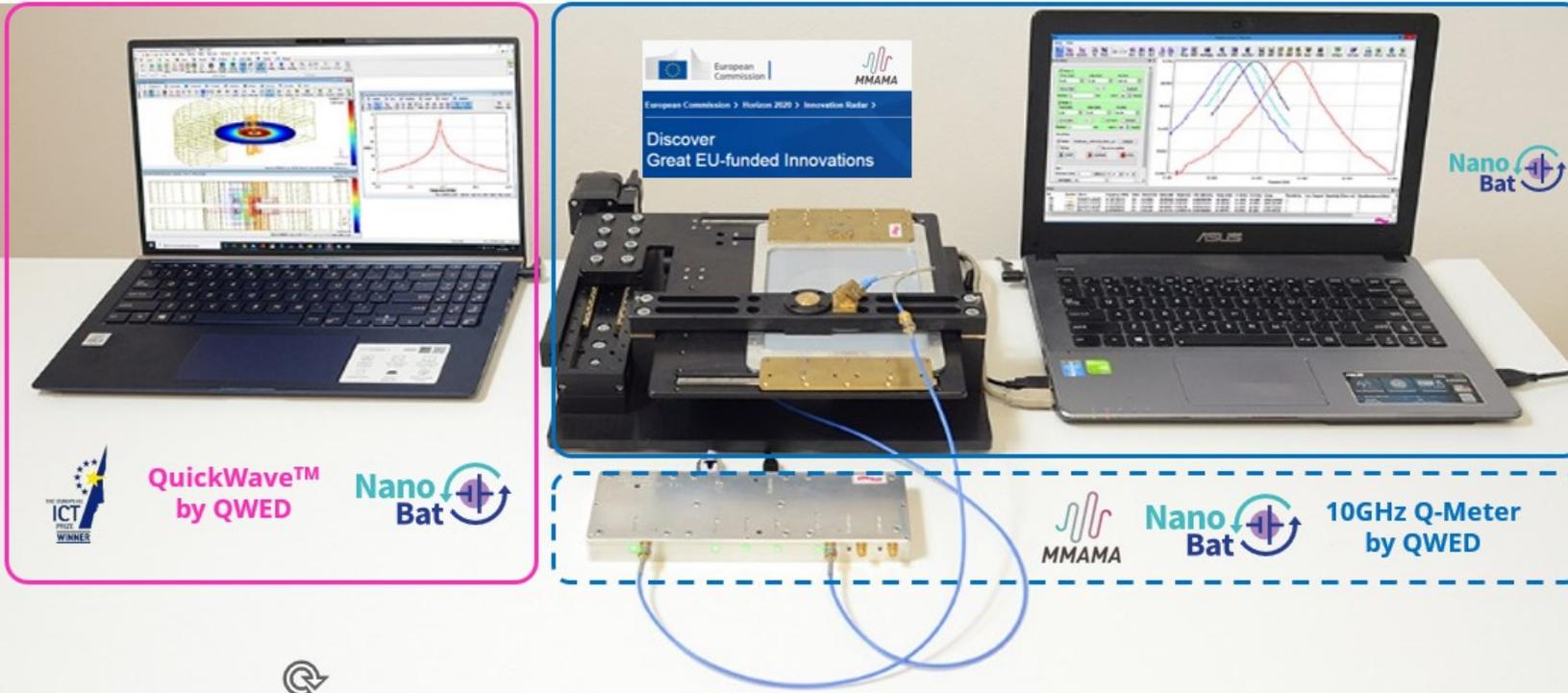
20 seconds



Exploring Synergies between Computer Modeling & Material Measurements



Twinned Modeling + Characterisation



- Originally designed for organic semiconductors (for solar cells)
- Widely used for various electronic materials (high-resistivity)
- Applicable to food packaging, glass, other materials relevant to MW heating systems

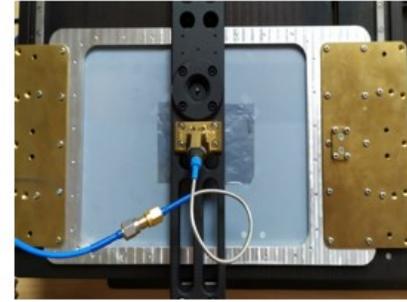
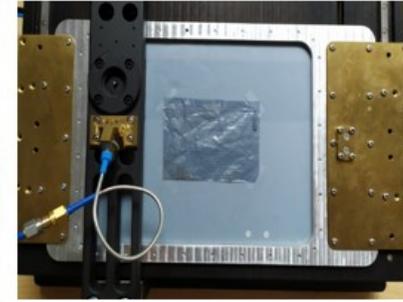
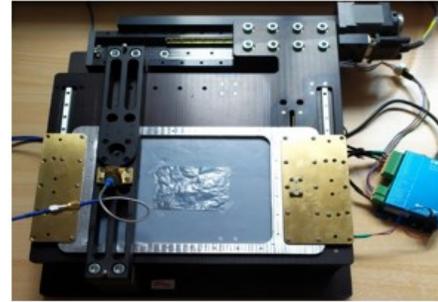
2D scanner designed with a modified 10 GHz SPDR

Finalist of the European Innovation Radar Prize 2021

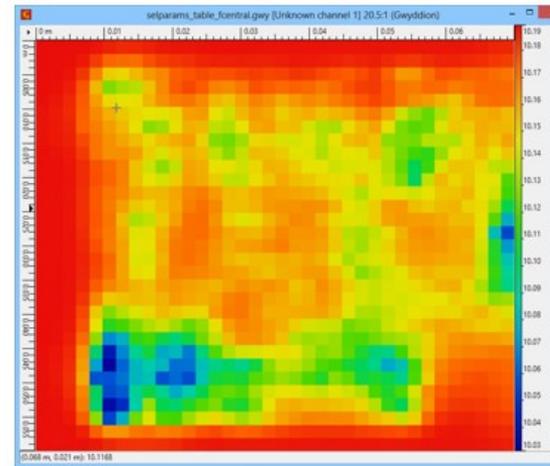
Example: unpopped & popped popcorn bag from ConAgra after Wikipedia



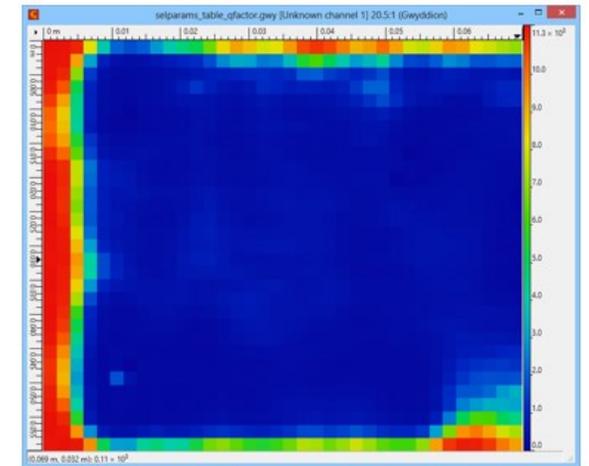
susceptor after 120sec of heating



Size of sample: 50mm x 70mm
Scan area: 60mm x 70mm
Scan step: 2mm
Scan results: 1116 (31 x 36)
Measurement: 500 freq points
Total scan time: 9053sec (150 min.)
One step time: 8.11sec.



Scan results of central frequency

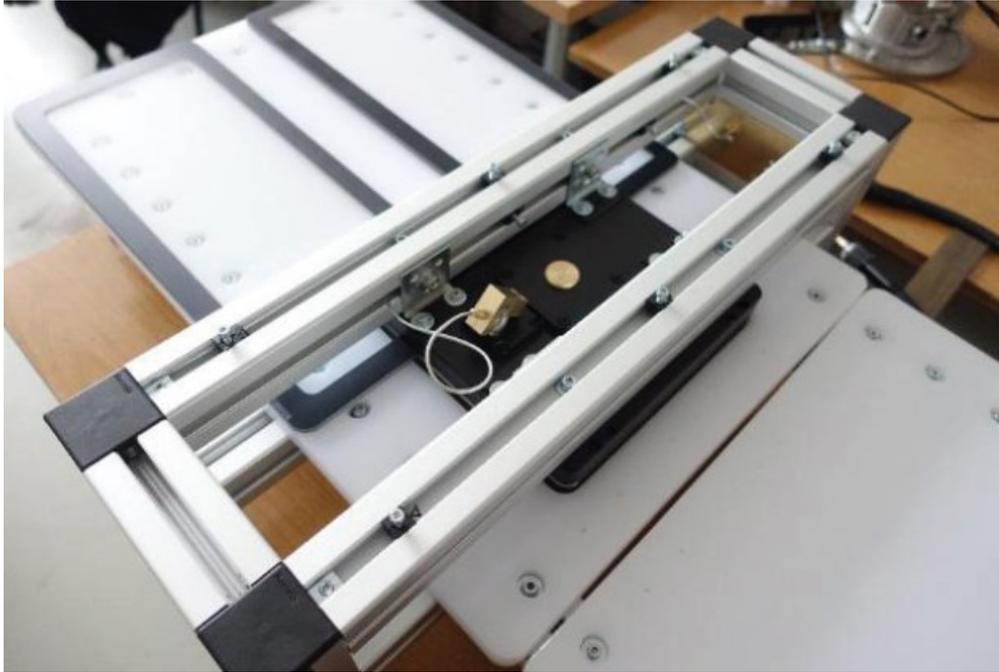


Scan results of Q-Factor

presented at:



17th International Conference
on Microwave and High Frequency Heating
9-12 September 2019, Valencia, Spain



2 GHz SPDR manual scanner
for MW oven glass panes

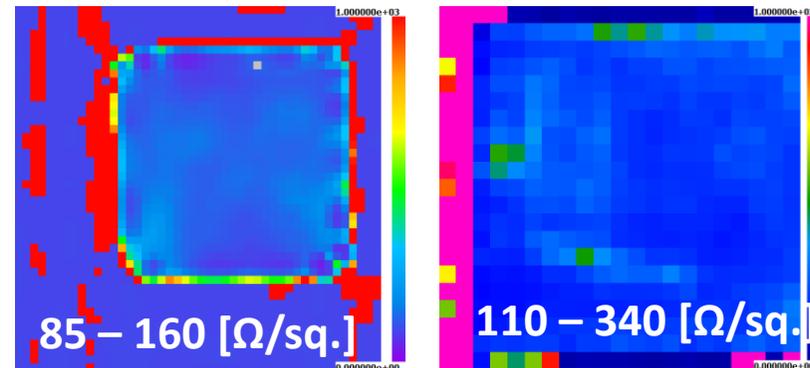
based on request by

B/S/H/

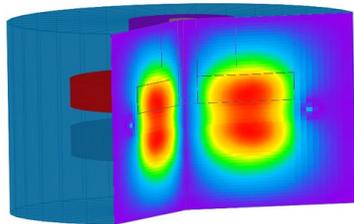


10 GHz SiPDR automatic scanner
for conductive sheets

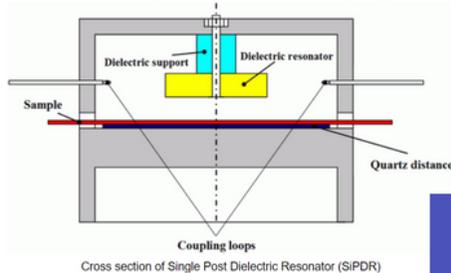
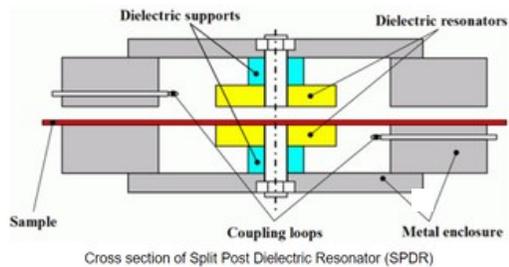
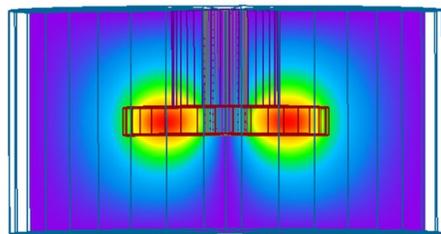
Surface resistance image of a battery anode
before & after cycling



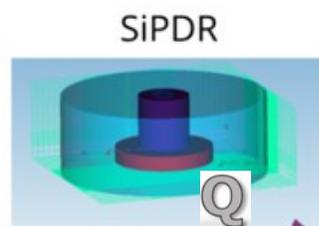
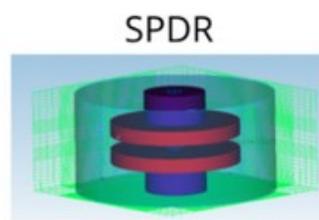
SPDR
Split-Post
Dielectric
Resonator



SiPDR
Single-Post
Dielectric
Resonator



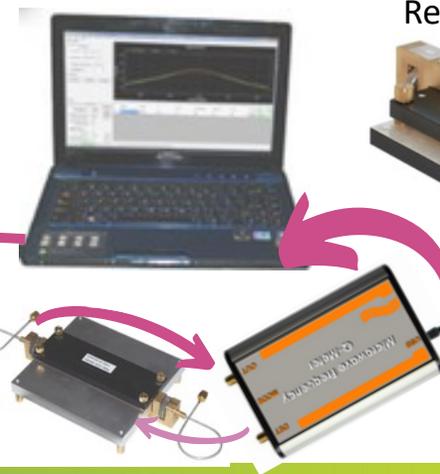
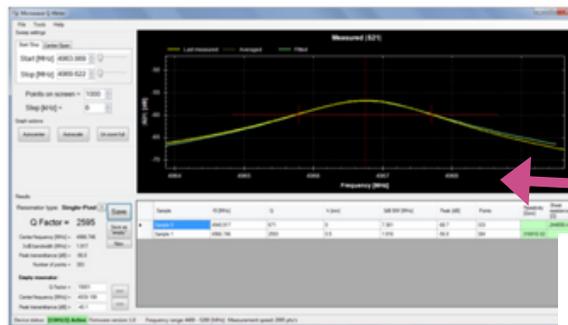
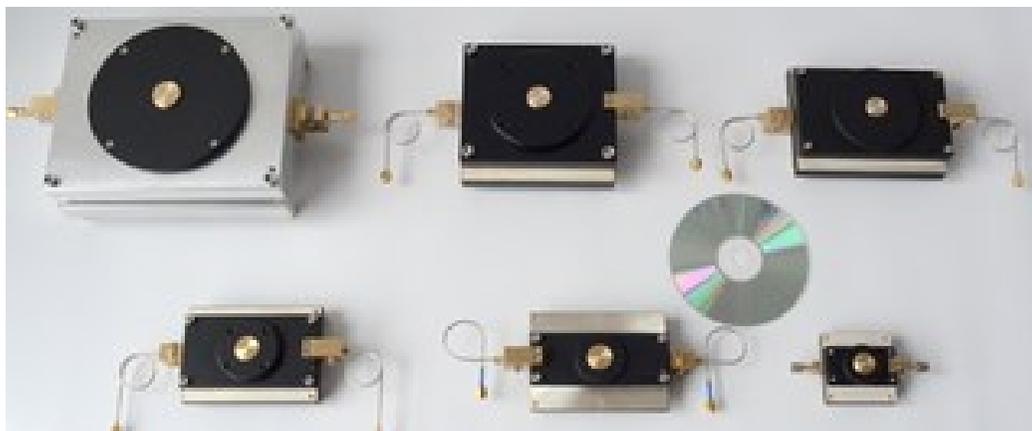
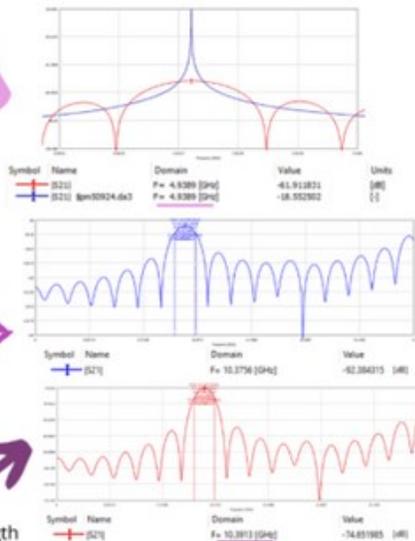
QuickWave
Modeller



QW

40 cells
per wavelength

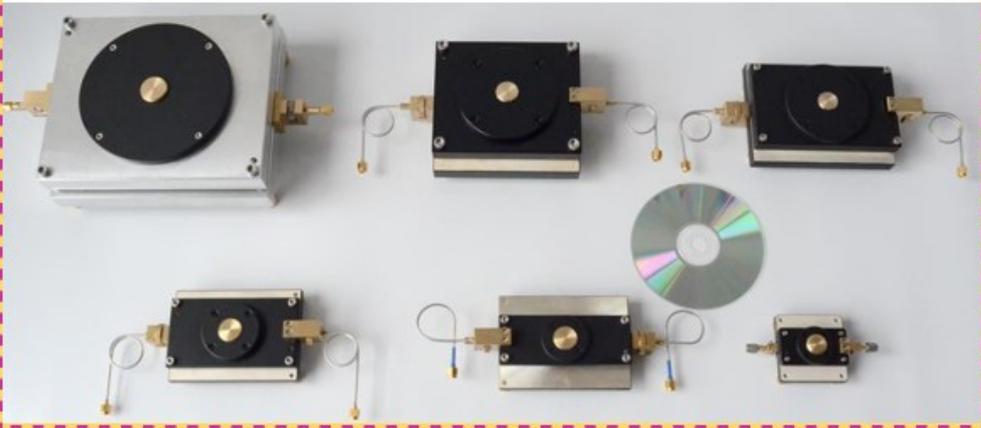
100 cells per wavelength



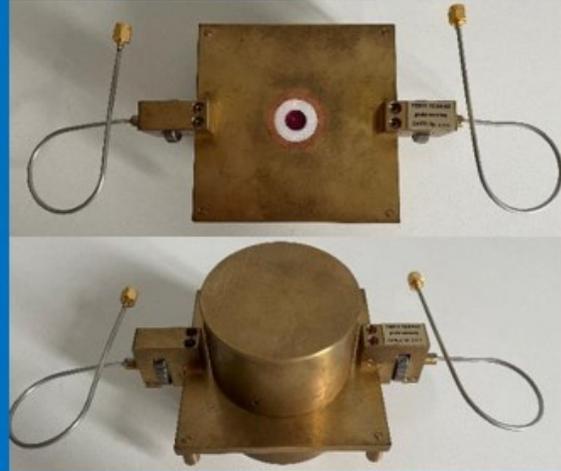
Split Post Dielectric
Resonator

Single Post Dielectric
Resonator

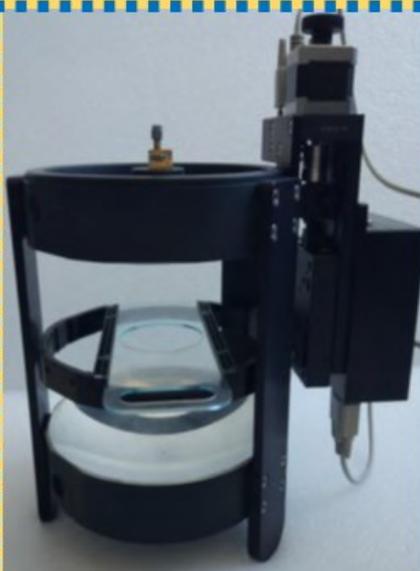
Split-Post Dielectric Resonator, typical units for 1.1 GHz -15 GHz for laminar low-loss dielectric materials



Sapphire Resonators (SaDR) for metal foils 13.5 / 20 GHz



more recent FPOR



Fabry-Perot Open Resonator automatic span, quasi-continuous 20 .. 120 GHz

5 GHz SiPDR for resistive sheets



TE01δ cavities, typically 1 GHz – 10 GHz for bulk low-loss dielectrics



LAMINAR LOW-LOSS DIELECTRICS

METALLIC OR RESISTIVE SHEETS

APPLIED IN TEMPERATURE-VARYING CONDITIONS



QWED's Popular Dielectric Resonators



Our project:
iNEMI

- 3M
- AGC-Nelco
- Ajinomoto USA
- AT&S
- Centro Ricerche FIAT-FCA
- Dell
- Dupont
- EMD Electronics (Co-Chair)
- Flex
- Georgia Tech
- **Showa Denko Materials**
- IBIDEN Co Ltd
- IBM
- **Intel**
- Isola
- ITRI (Co-Chair)
- **Keysight (Co-Chair)**
- MacDermid-Alpha
- Mosaic Microsystems
- **NIST**
- Nokia
- Panasonic
- **QWED**
- Shengyi Technology Company
- Sheldahl
- Unimicron Technology Corp
- Zestron



Sample Material Requirements

- Stable, Low loss
- Low moisture absorption / temperature dependency
- Isotropic
- Good mechanical & handling properties

Techniques Included

- Split Post Dielectric Resonator
- Split Cavity Resonator
- Fabry-Perot
- Balanced Circular Disk Resonator

→ Frequency Span : 10GHz – 100GHz with overlaps

10 Sample Kits Created

- Sample sizes 35 mm x 45 mm, 90 mm x 90 mm
- circulated between 10 labs

1st Project Stage

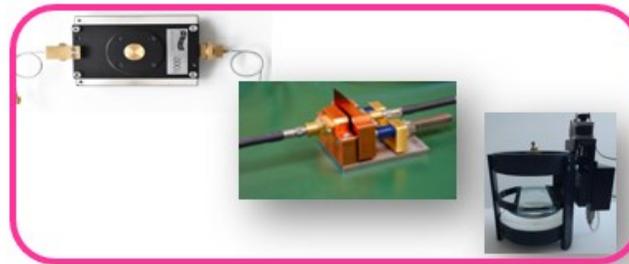
- Precision Teflon
- Cyclo Olefin Polymer

2nd Project Stage

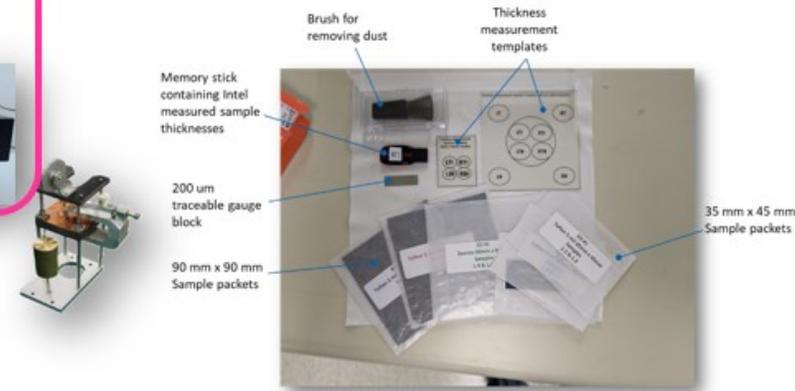
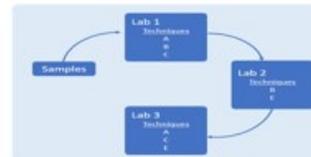
- Rexolite
- Fused Silica

Industrial

- Automotive



10 Laboratory Round Robin



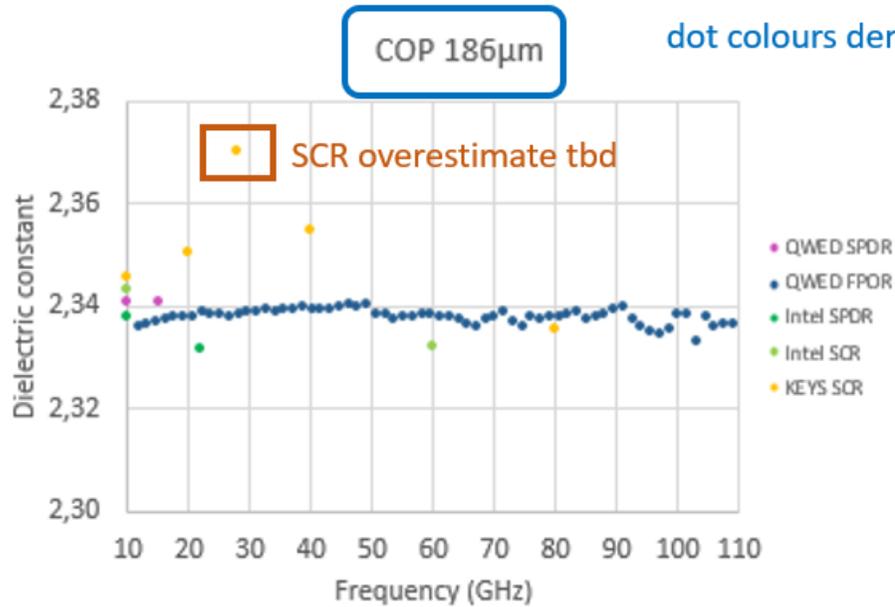
Note: the iNEMI benchmarking was aimed at 5G technologies, at higher than popular ISM frequencies, but its reference was 10GHz SPDR, which is of the same family as QWED's SPDRs covering 915MHz, 2.45 GHz and 5.8GHz bands.

A small but representative subset of the benchmarking results, (out of tens of thousands of measurement points)

3 labs, 3 techniques, 14 laboratory setups

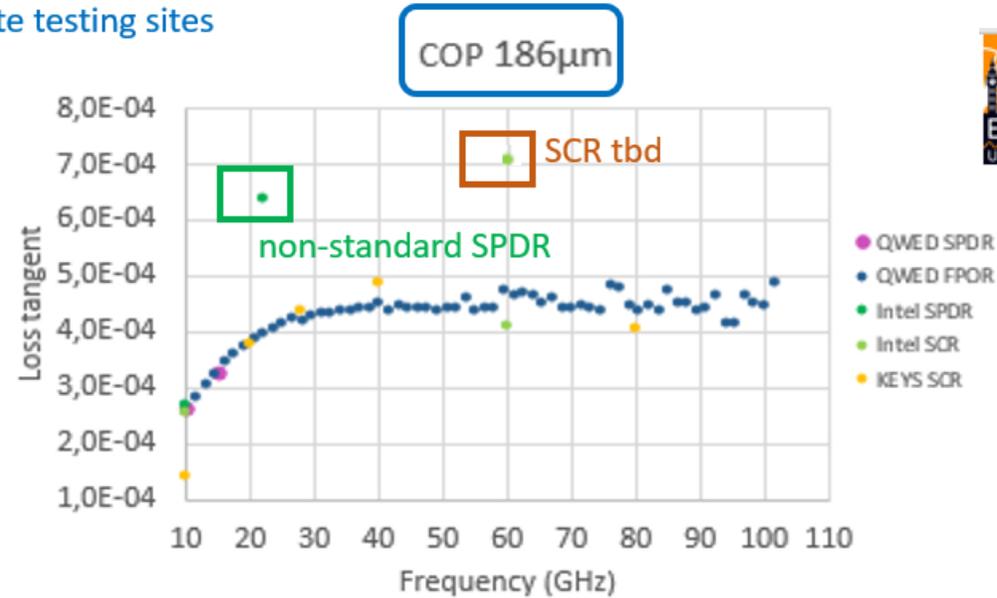
Intel - SCR at 10 / 60 GHz and SPDR at 10/ 20 GHz,
Keysight - SCR at 10 / 20 / 28 / 40 / 80 GHz
QWED - SPDR at 10/ 15 GHz and FPOR over 10-110GHz.

presented at:



Dk spread < 1% (within $\pm 0.5\%$ from average)
(< 2% incl. outliers)

dot colours denote testing sites



> 40GHz 2x increase in Df compared to 10GHz

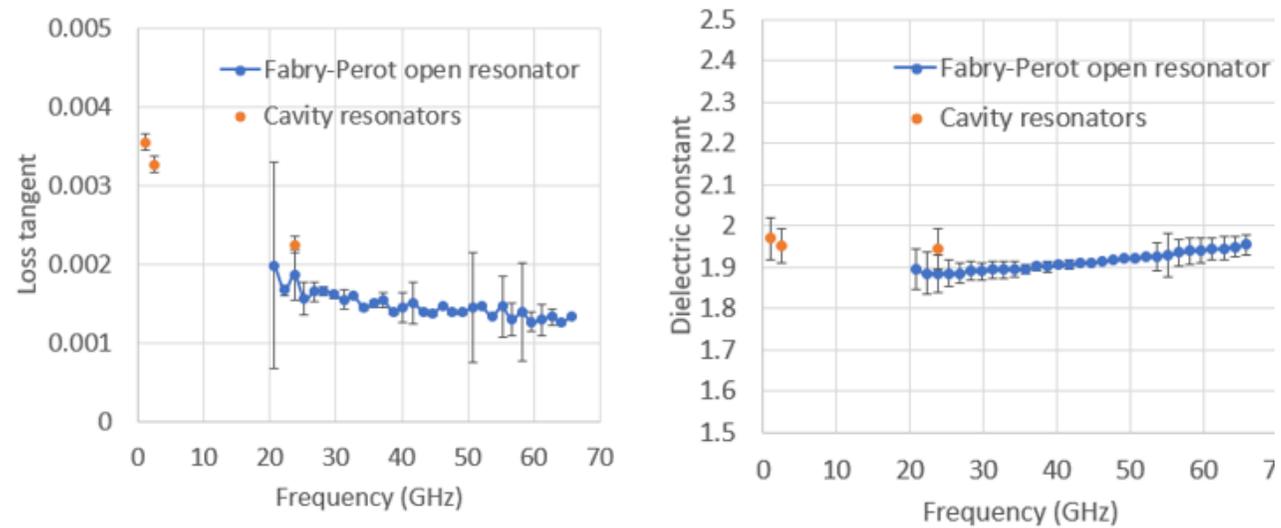


All data sets are available to iNEMI members
www.inemi.org

Note: the iNEMI benchmarking was aimed at 5G technologies, at higher than popular ISM frequencies, but its reference was 10GHz SPDR, which is of the same family as QWED's SPDRs covering 915MHz, 2.45 GHz and 5.8GHz bands.

- Customised to **low** or **high loss** materials
- Characterisation with **resonant methods**
 - **Cavity devices**
 - **Fabry-Perot Open Resonator (prototype)**
- Cavity fixtures available within **1 – 30 GHz**
- Cavity measurements at **varying temperature**
- FPOR targeted frequency range: 20 – 67 GHz

Popular coolant liquid



example cavities @1GHz & 24 GHz

FPOR



For more details, come to MicroAPPS:

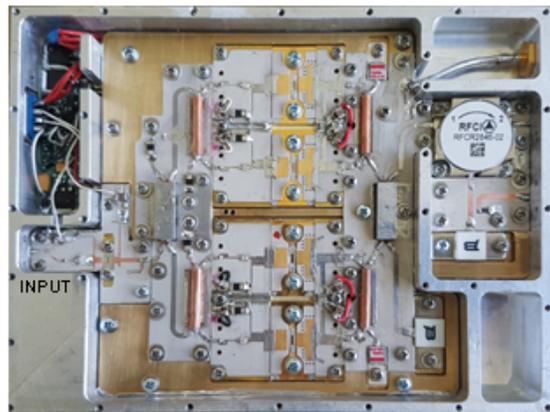
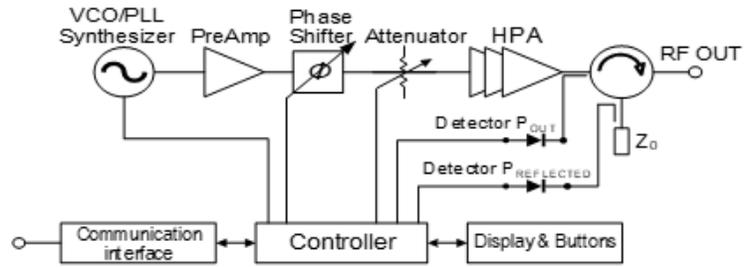
TUMA21

Tuesday, 14:30-14:45

MicroApps Theater, Booth 2447

or QWED Booth 2537 any time!

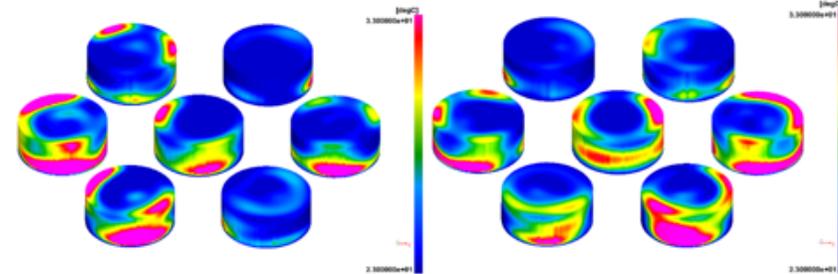
Solid-State Computer-Controlled Experimental Domestic Microwave Oven



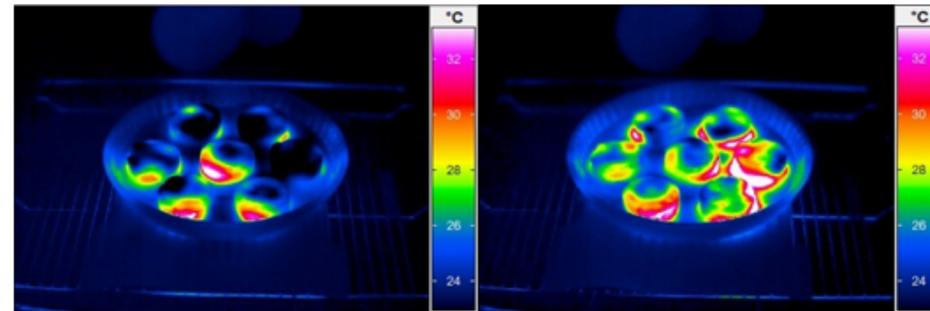
Output power measurement
OUTPUT
Reflected power measurement

Multifunctional heating source based on two-stage double-balanced GaN HEMT HPA (Prof. W.Wojtasiak, Dr. D.Gryglewski Warsaw Univ.Tech.)

Temperature in mashed potato cookies, after 60 s of heating, for different relative phase shifts (added 110 degrees) between two sources. (Development of packaging and products for use in microwave ovens, Elsevier, 2020)



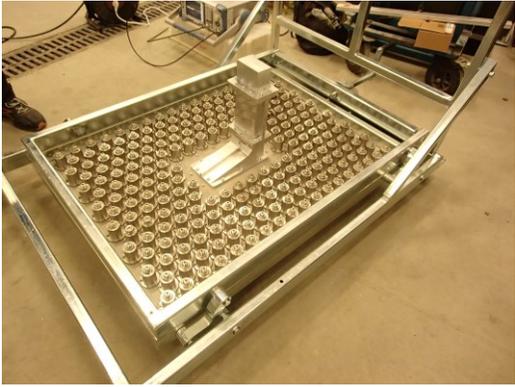
QuickWave modelling by QWED



Photos courtesy BSH HAUSGERATE GmbH, Traunreut, Germany.

B/S/H/

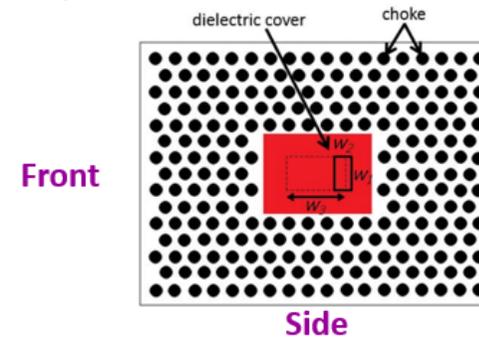
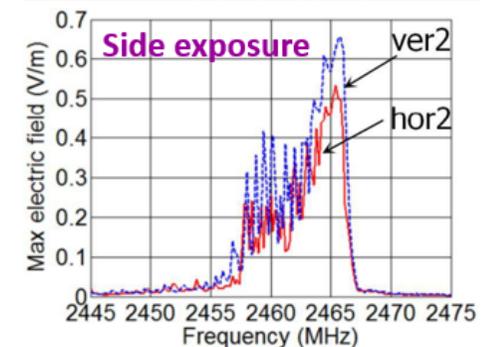
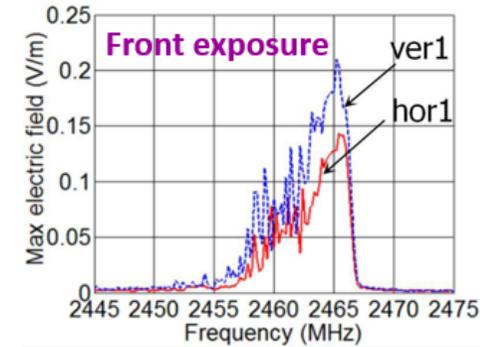
A Complete Design Cycle: Example 2



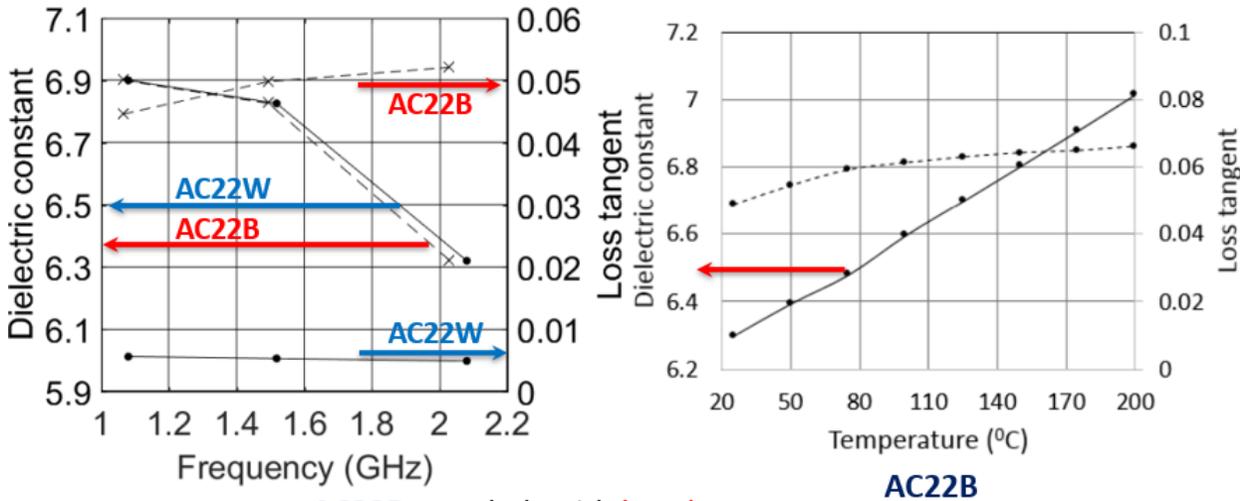
2.45GHz Aplicator for Road Repair (with Chokes & Full Safety System)



- Magnetron bandwidth: 10 MHz
- Front exposure ca. 9x smaller than side exposure
- EC recommendation: 10 W/m^2 (61 V/m)
- Power can be safely increased up to 30 kW and beyond



Measurements undertaken with **cavity resonators**.



AC22B – asphalt with **basalt** aggregates
AC22W – asphalt with **limestone** aggregates

Asphalt binder: $\epsilon_r = 2.65$, $\tan\delta = 0.00163$ @ 2.45GHz

Basalt aggregates: $\epsilon_r = 4.05$, $\tan\delta = 0.165$ @ 2.45GHz

presented at:



IMPI 56 Symposium
June 14 - 17, 2022
Savannah, Georgia, USA

- Computer Aided Design of microwave power systems requires creating a **Digital Twin** of the physical system. This is based on:
 - Physics Equations (and efficient solvers)
 - Material Relations (often with data coming from in-house measurements)
- Our **contributions to both above fields** have been presented, including:
 - modelling of multiphysics processes (radiation, fluid flow) with bilateral coupling
 - faster solvers (exploring structure symmetries – BoR or modern hardware)
 - new instruments for materials' characterisation: surface imaging, liquids, powders
- Our tools have been **applied to real-life problems** provided by our industrial and project partners, which we kindly acknowledge.

The relevant work of QWED team is currently co-funded by:



the *Polish National Centre for Research and Development* under contracts
M-ERA.NET2/2020/1/2021 and *M-ERA.NET3/2021/83/I4BAGS/2022*.



M-ERA.NET 3 has received funding from the *European Union's Horizon 2020*
research and innovation programme under grant agreements *No 958174*.

ULTCC6G_EPac



We kindly acknowledge the collaborations with our partners in the above European projects.



We acknowledge the iNEMI “5G” partnerships for round-robin experiments and discussions.

Special thanks to all our industrial clients and partners for driving our developments and their kind permission to publish selected industrially-representative results.

Thank you for your attention!

1997: QWED founded
1998: Prime Minister Award

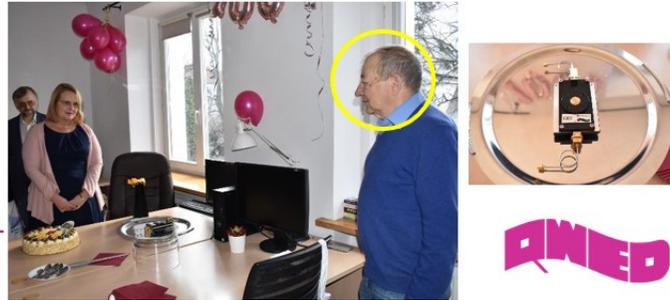


Prof. Jerzy Buzek awarding QWED team in 1998
Prime Minister of Poland 1997-2002
President of the European Parliament 2009-2012

2022: our 25 years



2020: sale of our 1000th resonator



meet QWED team in Booth #2537



mceluch@qwed.eu

www.qwed.eu

[1] P.O. Risman, "A Microwave Oven Model – Examples of Microwave Heating Computations", *Microwave World*, 19(1), 1998, pp. 20-23.

[2] U. Erle, P. Pesheck, and M. Lorence, "Development of packaging and products for use in microwave ovens", 2nd edition, Elsevier 2020:

Chapter 18: M. Celuch, P. Kopyt, and M. Olszewska-Placha, "Modeling of cavities and loads with FDTD and FEM methods", pp. 459-512.

Chapter 19: M.Celuch and M.Olszewska-Placha, "Space-discrete electromagnetic modelling of microwave susceptors", pp. 513-530.

Chapter 20: M.Celuch, W.Gwarek, and M.Olszewska-Placha, "Modelling of excitation in domestic microwave ovens", pp. 531-556.

[3] P.O. Risman, Huskvarna, Sweden, Microwave Heating Apparatus, United States Patent, Appl. No.: 974,606,1981