

ELECTRONIC MATERIALS AND APPLICATIONS (EMA 2021)

The American Ceramic Society
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How to support 5G materials measurements, antenna designs, and standards developments with QuickWave simulations

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S13 – 5G Materials and Applications
Telecommunications
22 Jan 2021



Outline

1. Electromagnetic modelling & simulations – development & applications by QWED.
2. Modelling-based characterisation techniques for 5G materials.
3. Electromagnetic design of 5G antennas.
4. Modelling of mm-wave interactions with tissues (for standards' developments).
5. Conclusions & outlook.

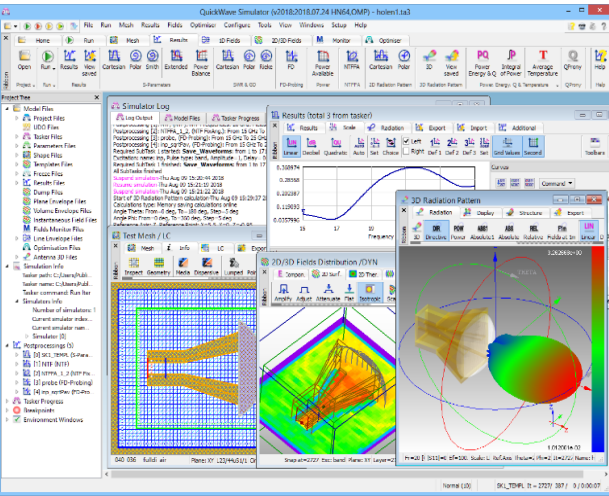




Polish high-tech SME - 23 years on the world's market

R&D projects

Business branches presented annually at IEEE IMS Show

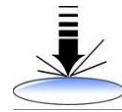


Electromagnetic simulation & design software, 3D & BOR 2D tools

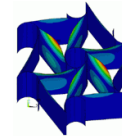
based on 300+ publications by:
prof.W.Gwarek, IEEE Fellow, DML, Pioneer Award
dr.M.Celuch, President of QWED



PREZES RADY MINISTRÓW
przyznaje III nagrodę
za wybitne krajowe osiągnięcia naukowo-techniczne
zpolemni Polnischki Warszawskiej w składzie:
dr inż. Malgorzata CELUCH-MARCYSIAK, dr inż. Maciej STPIEWSKI,
dr inż. Andrzej WIECZORSKI
pod kierownictwem: prof. dr hab. inż. Wojciecha GWAREKA



FP6 SOCOT – development and validation of an optimal methodology for overlay control in semiconductor industry, for the 32 nm technology node and beyond.



FP6 CHISMACOMB – development, modelling, and applications of chiral materials → EM validation of mixing rules



Eureka E! 2602 MICRODEFROST MODEL – innovative software-based product development tool for simulating and optimising heating and defrosting processes in microwave ovens



FP7 HIRF SE (High Intensity Radiated Field Synthetic Environment) - numerical modelling framework for aeronautic industry



Eureka FOODWASTE – developing new microwave treatment system for high water content waste



ERA-NET MNT NACOPAN – applications and modelling of nano-conductive polymer composites



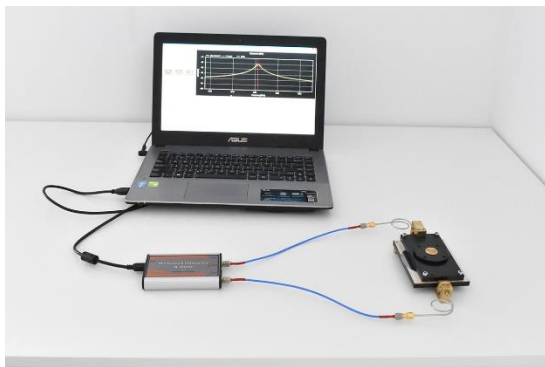
NGAM2 – designing an industrial device for thermal bonding of bituminous surfaces with the aid of microwave heating



MMAMA (Microwave Microscopy for Advanced and Efficient Materials Analysis and Production) – accelerating the development of high efficiency solar cells through application and enhancement of material measurement techniques



NanoBat - developing a novel nanotechnology toolbox for quality testing of Li-ion and beyond Lithium batteries with the potential to redefine battery production in Europe and worldwide.

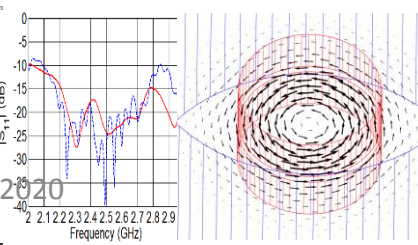


Test-fixtures for precise material measurements based on 300+ publications by prof.J.Krupka, IEEE Fellow



Consultancy & design services based on EM expertise & tools

team of 10+engineers, 4 PhDs, 2 Profs
key areas: MW power appliances, customised resonators, antennas & feeds



Modelling – based characterisation of 5G materials

Focus on dielectric resonators:

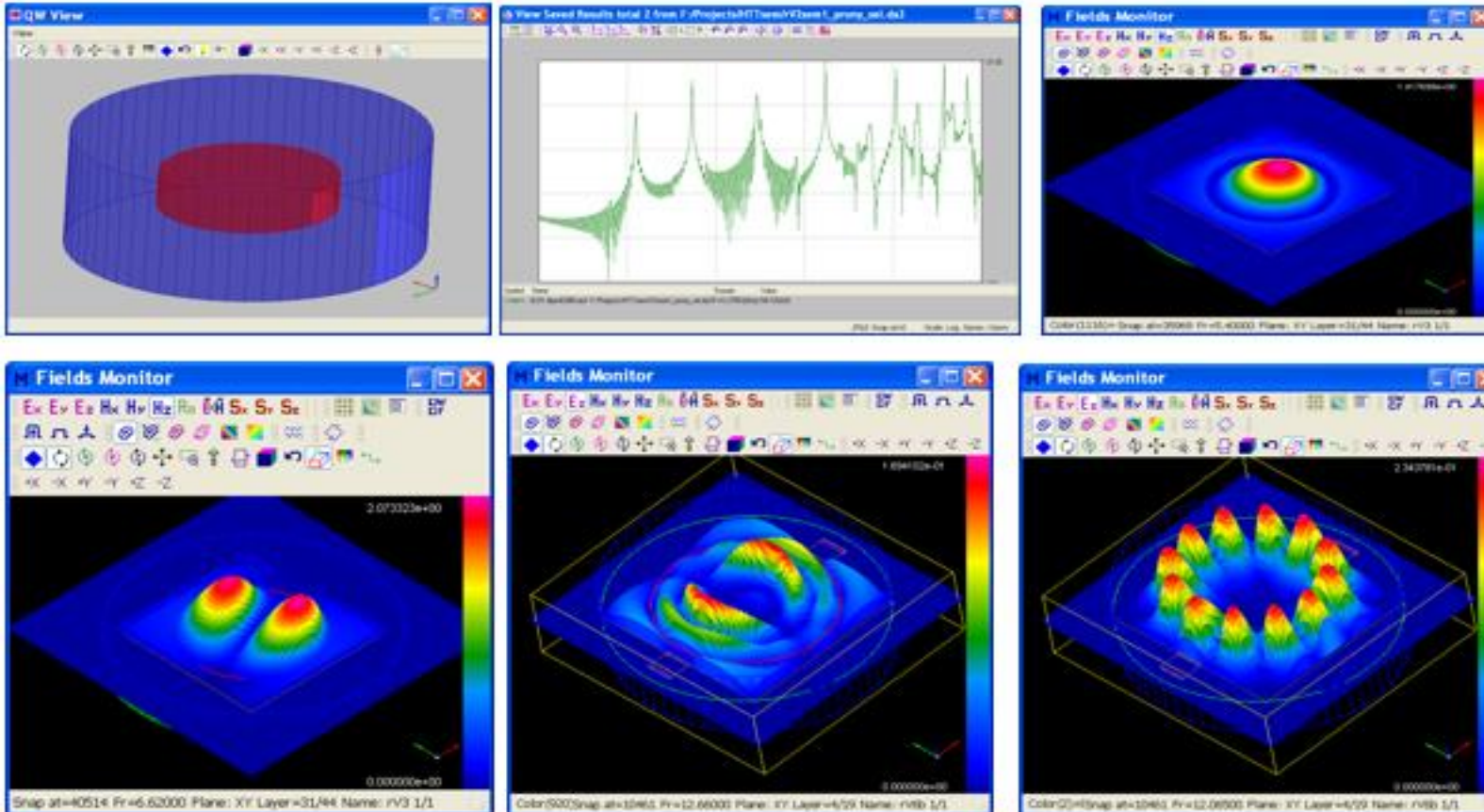
- proven ultra-high accuracy in GHz range (0.3% for Dk, IEC 61189-2-721:2015)
- dedicated to low-loss materials & thin material sheets
- ease-of-use
- available on the market
- repeatability & reproducibility for 5G under independent studies (iNEMI project)



How do dielectric resonators work



Dielectric resonator (top left)
as a multimode device (see transmission diagramme, top centre)
including TE₀₁ mode (top right) and many higher modes (lower row)

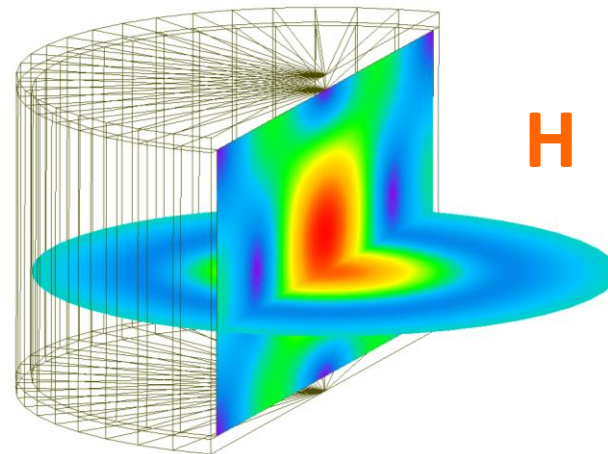
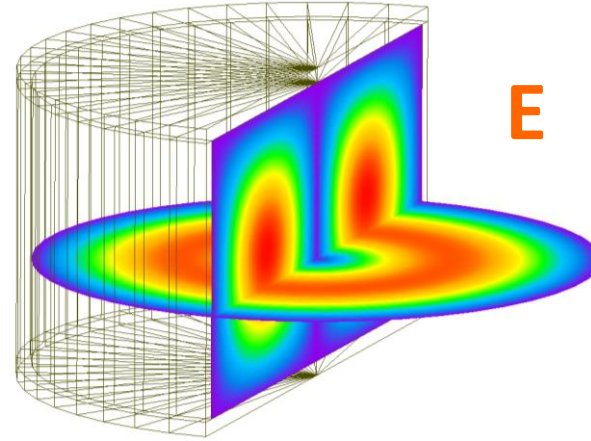


What is RESONANCE

Eigenvalue problem in theoretical electromagnetics:

- Non-zero electromagnetic fields (non-zero energy) exist in a region without any energy exchange with the outside (no "feeding").
- This is mathematically possible at specific frequencies (**eigenfrequencies**). The corresponding spatial field patterns are called modes (**eigenmodes**).
- In a lossless region, the fields exist ("ring") *ad infinitum* (**sinusoidal oscillations**).
- If there are (not-too-high) losses in the region, the fields are gradually damped (**damped sinusoidal oscillations**) with damping characterised by quality factor (**Q-factor**) and frequency little altered (compared to the same materials with losses neglected).

Example: TE₀₁₁ mode in cylindrical cavity



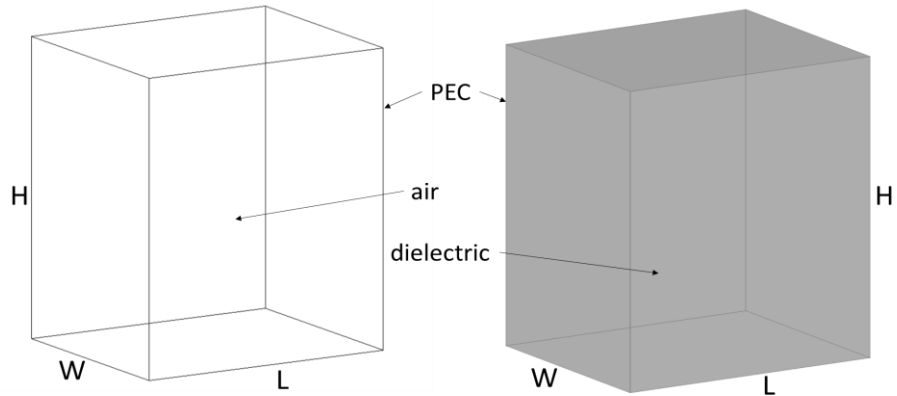
Resonance problem in applied electromagnetics:

- There is feeding from the outside, but the **coupling** is non-too-strong.
- The corresponding **resonant frequencies** are close to eigenfrequencies of the corresponding isolated problem.
- Energy loss in a lossy resonating region is **compensated** with energy supplied by the feed. Energy is also lost on internal losses (resistance) of the feed.



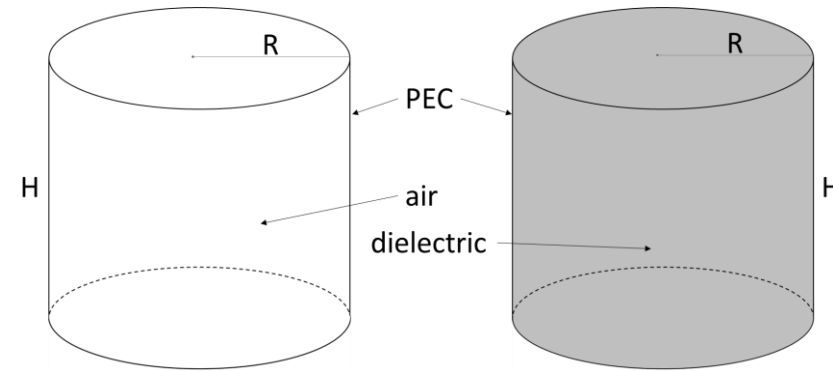
Canonical examples of resonators

Eigenvalue problems: analytical solutions exist for **cuboidal** and **cylindrical** cavities:



$$Q = 2\pi \frac{\overline{W}}{P_q T}$$

$$Q = 2\pi \frac{\iiint_V \epsilon \vec{E} \cdot \vec{E}^* dv}{T \iiint_V \sigma \vec{E} \cdot \vec{E}^* dv} = \frac{\omega \epsilon}{\sigma} = \frac{1}{\tan \delta}$$



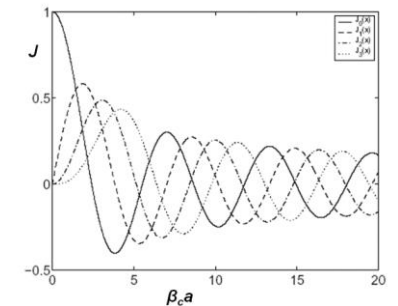
*in non-magnetic
low-loss dielectrics*

$$f_{r,mnp} = \frac{v}{2} \sqrt{\left(\frac{m}{W}\right)^2 + \left(\frac{n}{L}\right)^2 + \left(\frac{p}{H}\right)^2}$$

$$v = \frac{1}{\sqrt{\mu \epsilon}} = \frac{c}{\sqrt{\epsilon_r}}$$

$$f_{r,mnp} = \frac{v}{2} \sqrt{\left(\frac{\kappa_{mn}^{(i)}}{\pi R}\right)^2 + \left(\frac{p}{H}\right)^2}$$

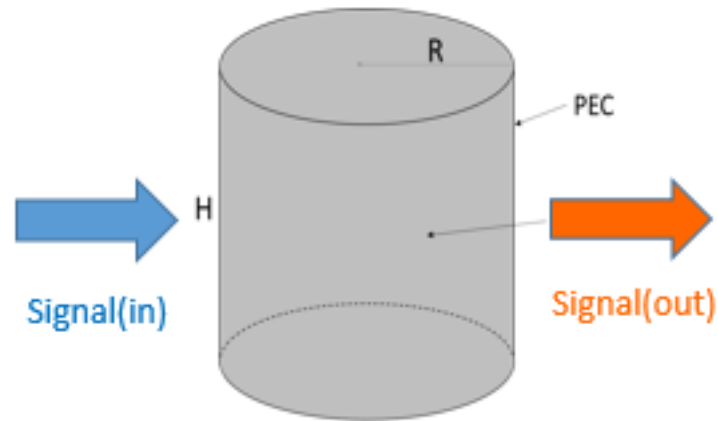
→ application of cavities to Dk measurements appears straightforward!
(but cavity losses should be minimised)



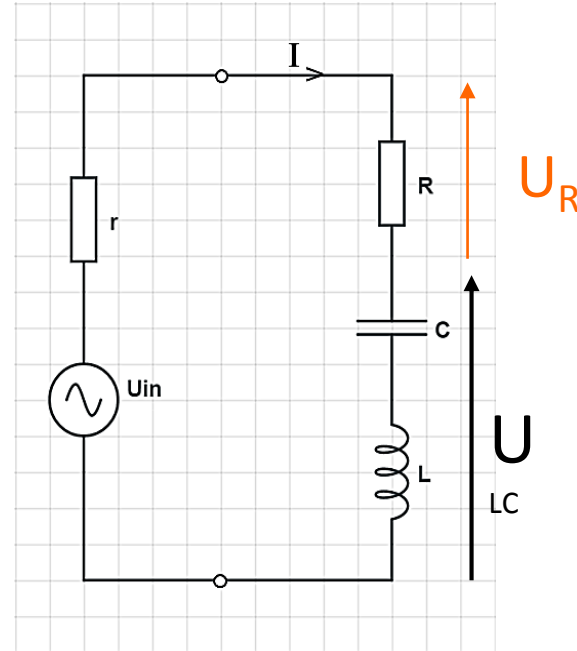
Canonical examples of resonators

Analytical solutions are for **eigenvalue** problems.

Measurement problems are **deterministic** (cavity is **coupled** to source & load).



given fixed strength of **Signal(in)**,
at resonance **Signal(out)** is strongest

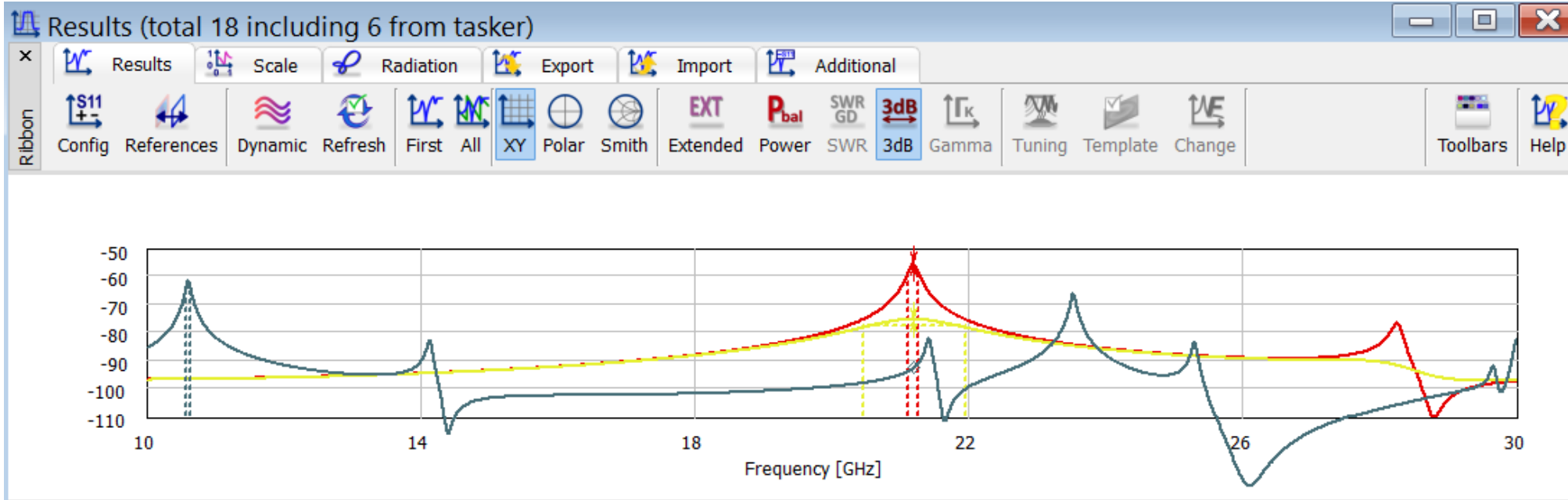
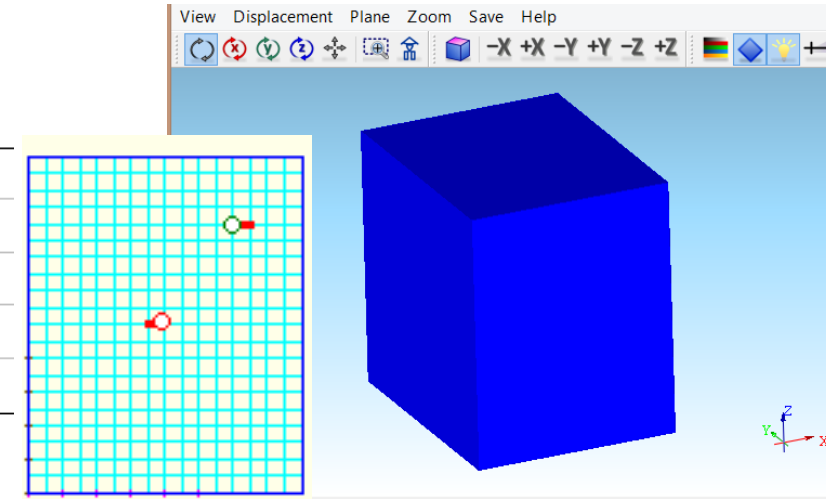
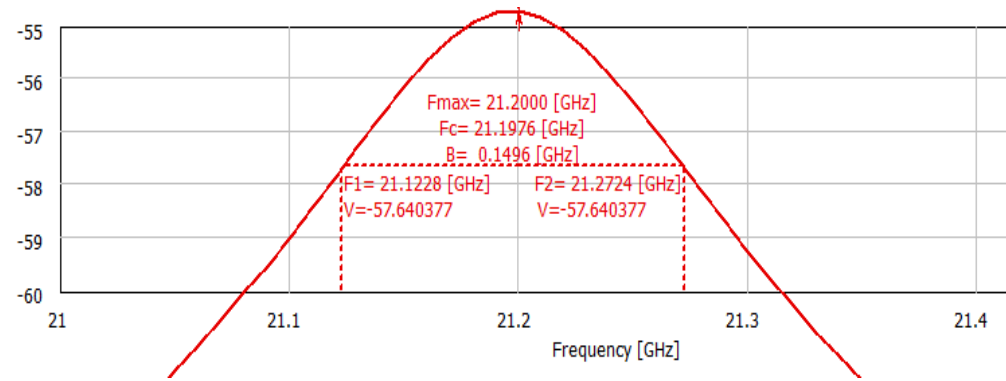


given fixed strength of U_{in} ,
at resonance U_R is strongest ($U_{LC} = \text{zero}$)



QuickWave model of a cuboidal cavity

Transmission $|S_{21}|$ simulated between weakly coupled source and probe in a cube $8 \times 10 \times 10$ [mm]



$$\epsilon_r = 1 \quad \sigma = 0.00833 \text{ S/m}$$

@21.2GHz:

$$\tan \delta = 0.071$$

$$Q_{SUT} = 1 / 0.0071 = 141$$

$$Q_{S21} = 21.2 / 0.1496 = 141$$

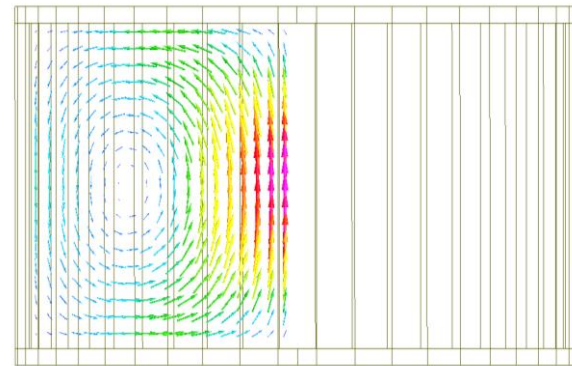
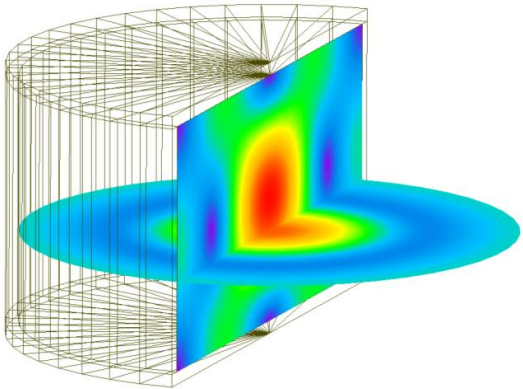
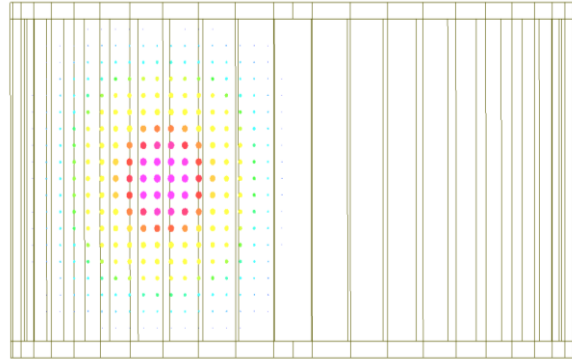
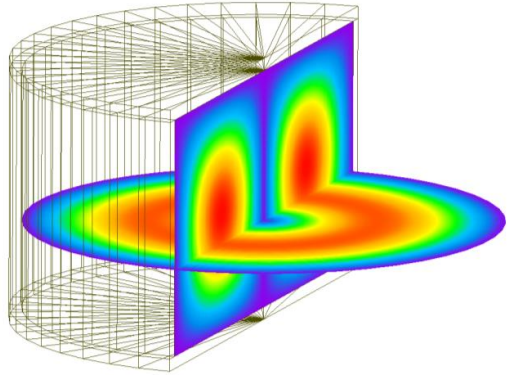
$$\epsilon_r = 1 \quad \sigma = 0.0833 \text{ S/m}$$

$$\epsilon_r = 4 \quad \sigma = 0.0166 \text{ S/m}$$

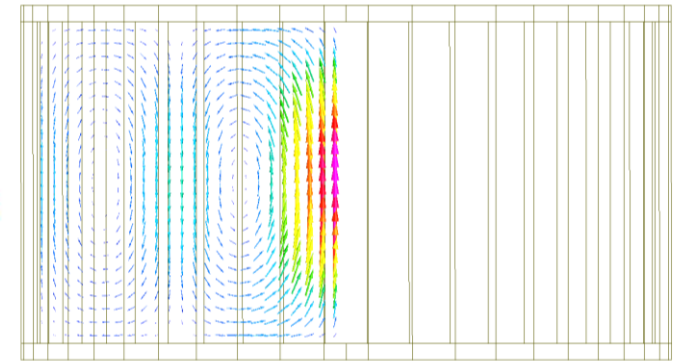
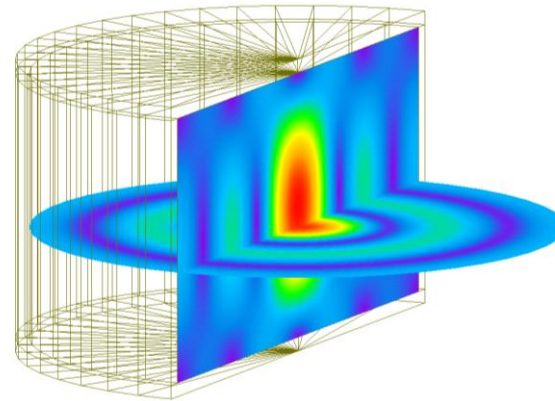
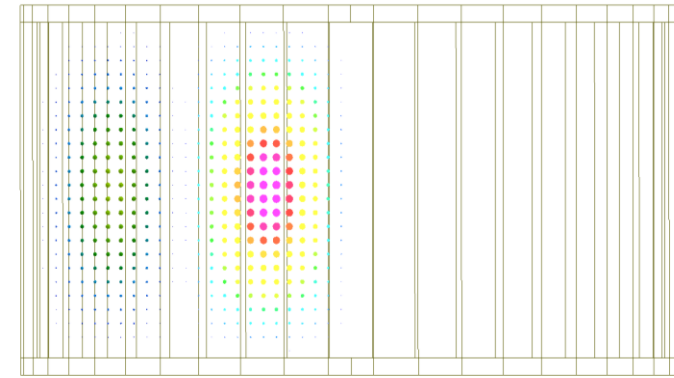
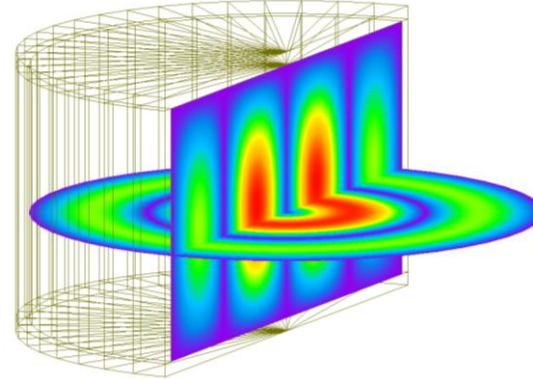


QuickWave model of a cylindrical cavity

TM₀₁₁ mode



TM₀₂₁ mode



compared to rectangular (cuboidal) cavities, typically:

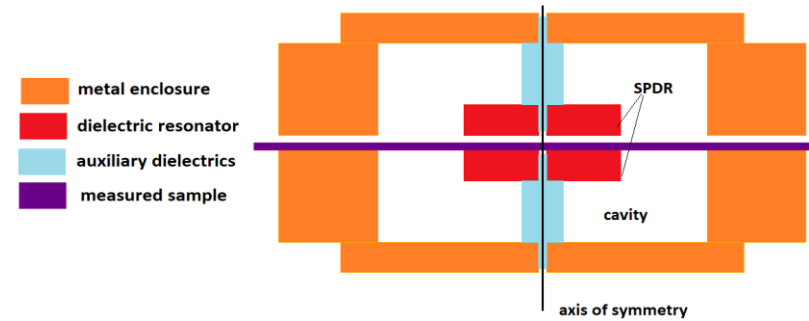
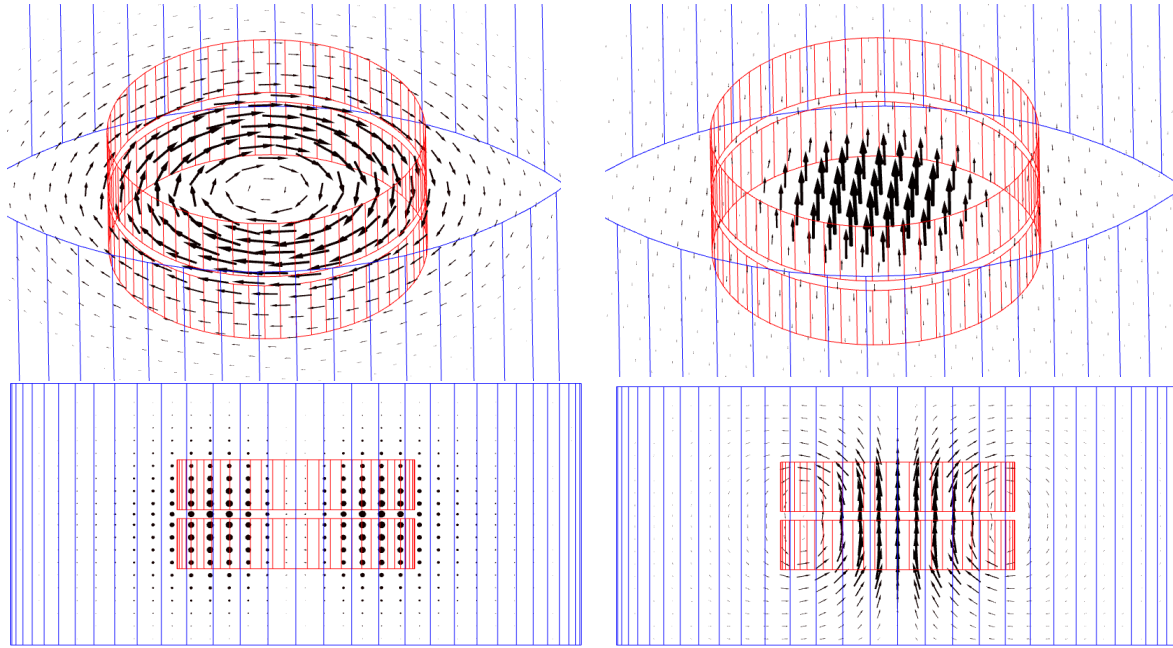
- lower contribution of wall losses
- easier standard manufacturing



Split-Post Dielectric Resonator method

E-field

H-field



- resonant mode with EM fields mostly confined in and between those ceramic posts → **minimal losses in metal enclosure**
- H-field is only vertical at the side wall of the enclosure → only circumferential currents in side wall → **no radiation through slot**
- E-field tangential to SUT → **air slots between SUT and posts have negligible effect**
- **easy SUT insertion through slot, no dismatling, NDT method**
- all EM energy injected through the coupling loops is contained within in the SPDR “head” (inside the enclosure)
- an estimated 95% of energy confined in and between the ceramic posts
- **once-in-a-lifetime calibration sufficient for general materials (NOTE: new calibration services dedicated to 5G coming soon!)**



Split-Post Dielectric Resonator method

SUT of $\epsilon_s = \epsilon_s' - j \epsilon_s''$ is inserted into DR:
 resonant frequency changes from f_e to f_s
 Q-factor changes from Q_e to Q_s .

$$\frac{f_e - f_s}{f_e} \approx \frac{h}{2C} \iint_S [\epsilon_s'(x, y) - 1] |E(x, y)|^2 dS$$

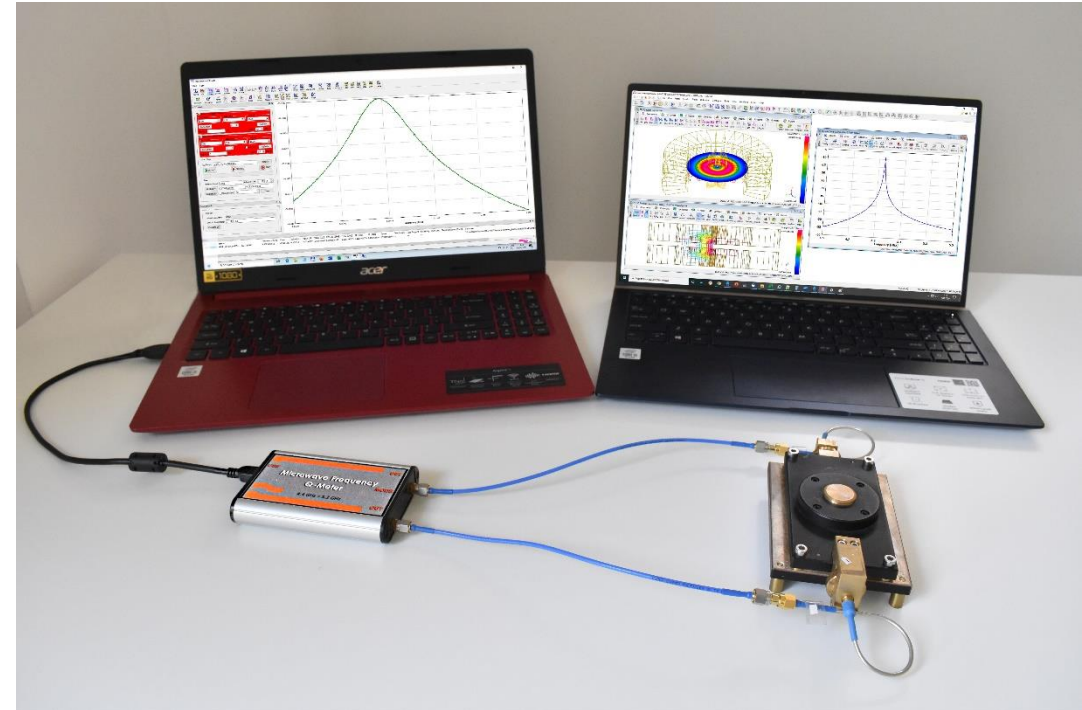
$$\frac{1}{Q_s} - \frac{1}{Q_e} \approx \frac{h}{C} \iint_S \epsilon_s''(x, y) E^2(x, y) dS$$

$$C = \iiint_V |E(x, y)|^2 dV$$

field assumed invariant in z-direction

S is called the DR's *head*

sign \approx reflects field pattern changes caused by SUT

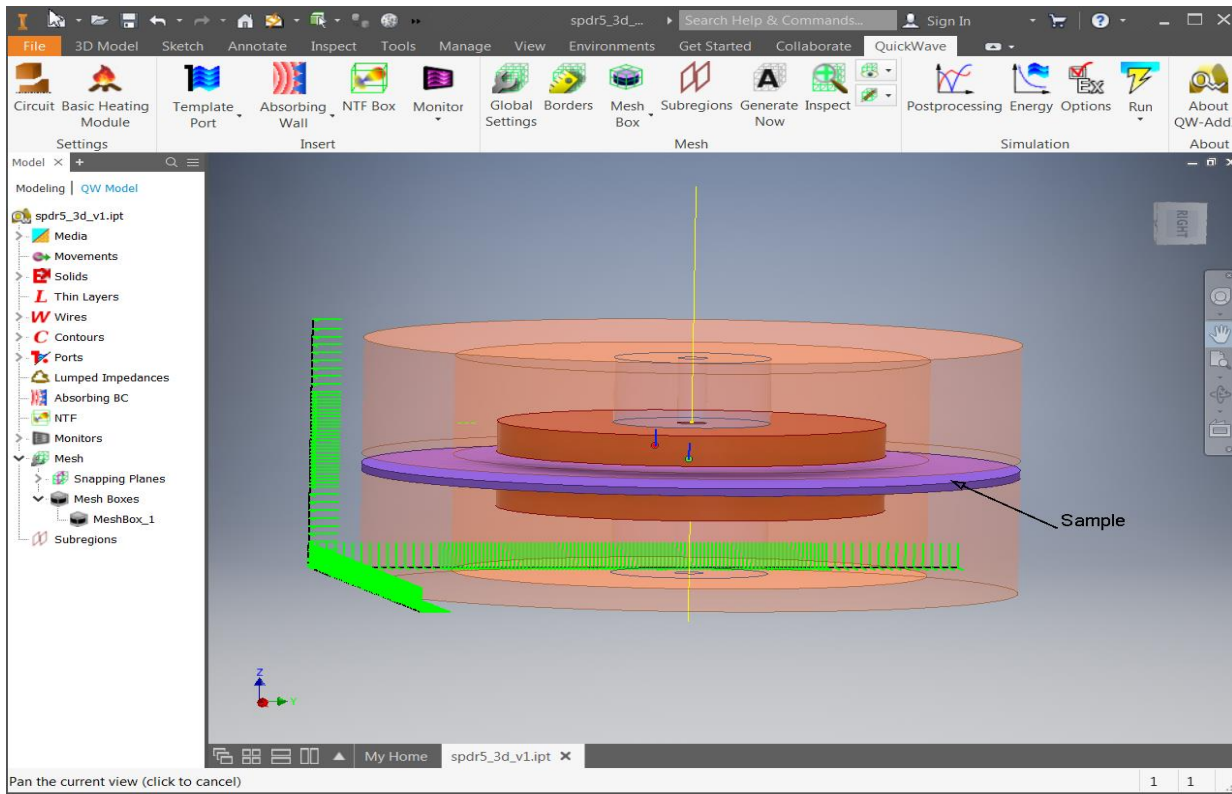


calibration (**based on modelling**)
 minimises effects of:

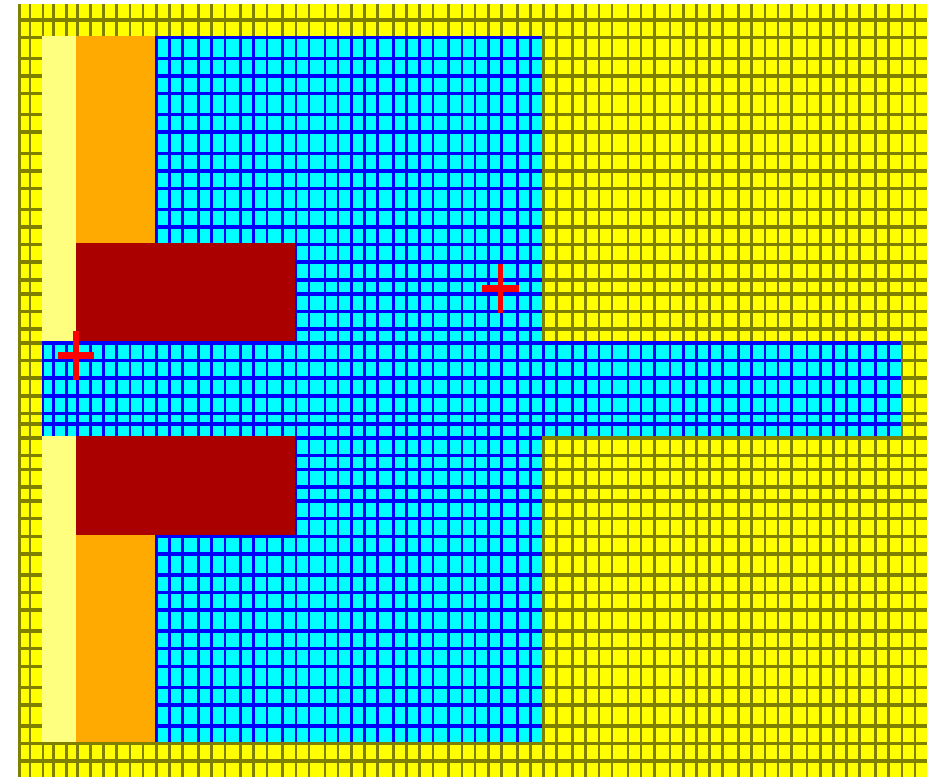
field variation in z
 field changes due to SUT
 manufacturing tolerances



QuickWave modelling of SPDR

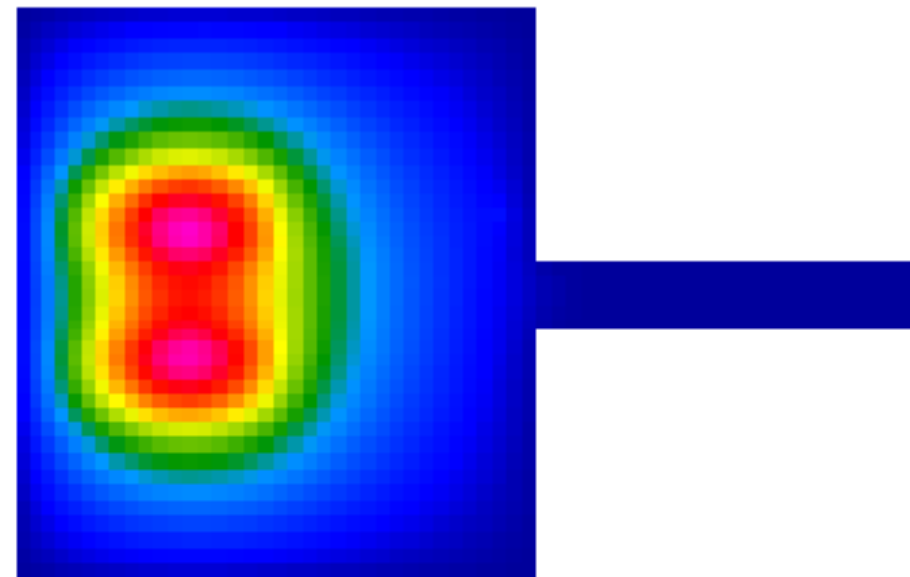
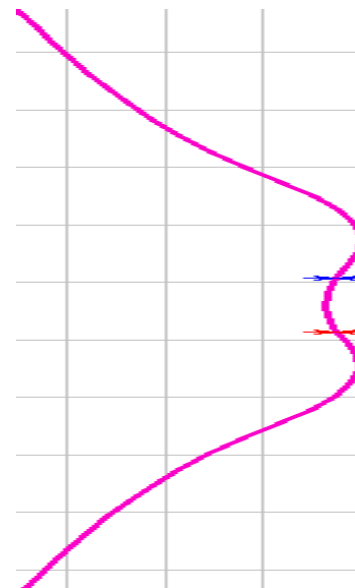
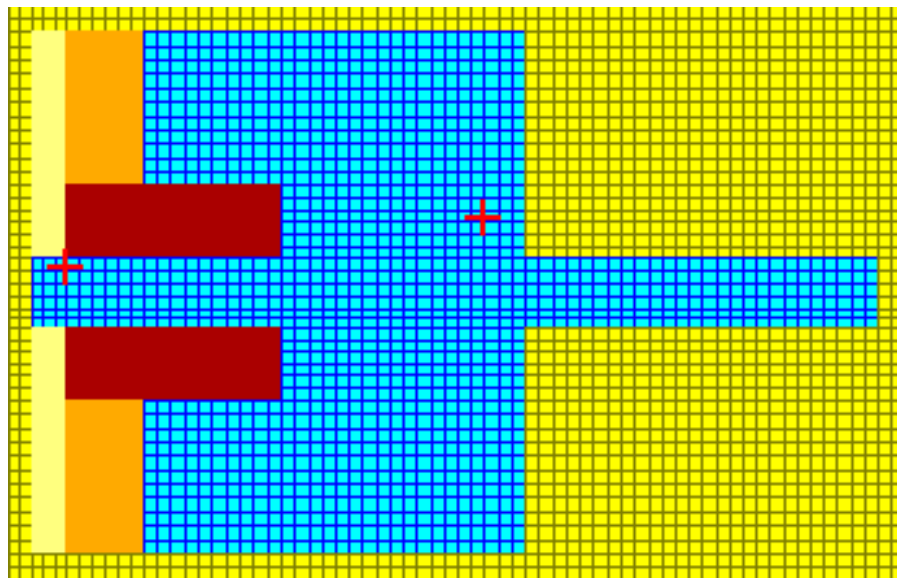


Full **3D model** of 10GHz SPDR
in **QW-AddIn** for Autodesk® Inventor® Software
(common environment for modelling & manufacturing)



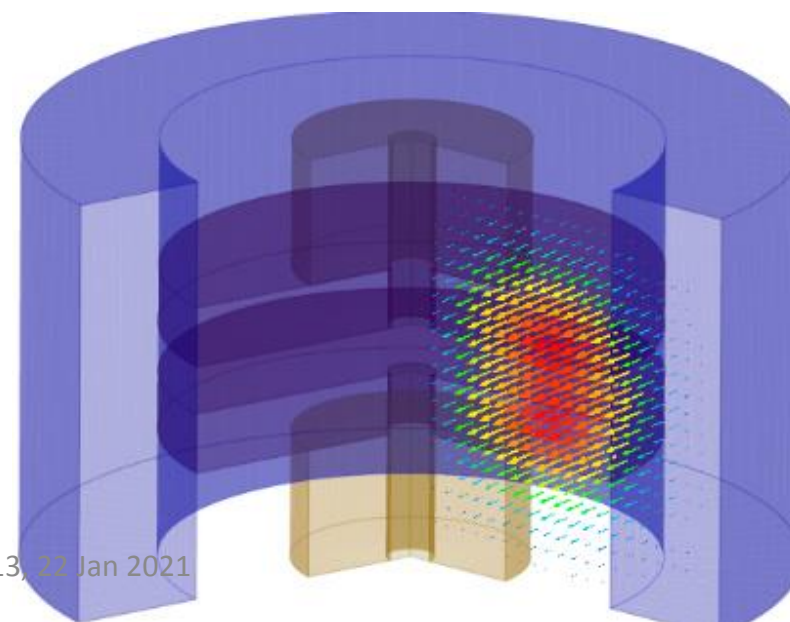
Axisymmetrical **2D BOR** model
full EM information
economies in computer effort : 10^3 or more

QuickWave model of SPDR field distribution

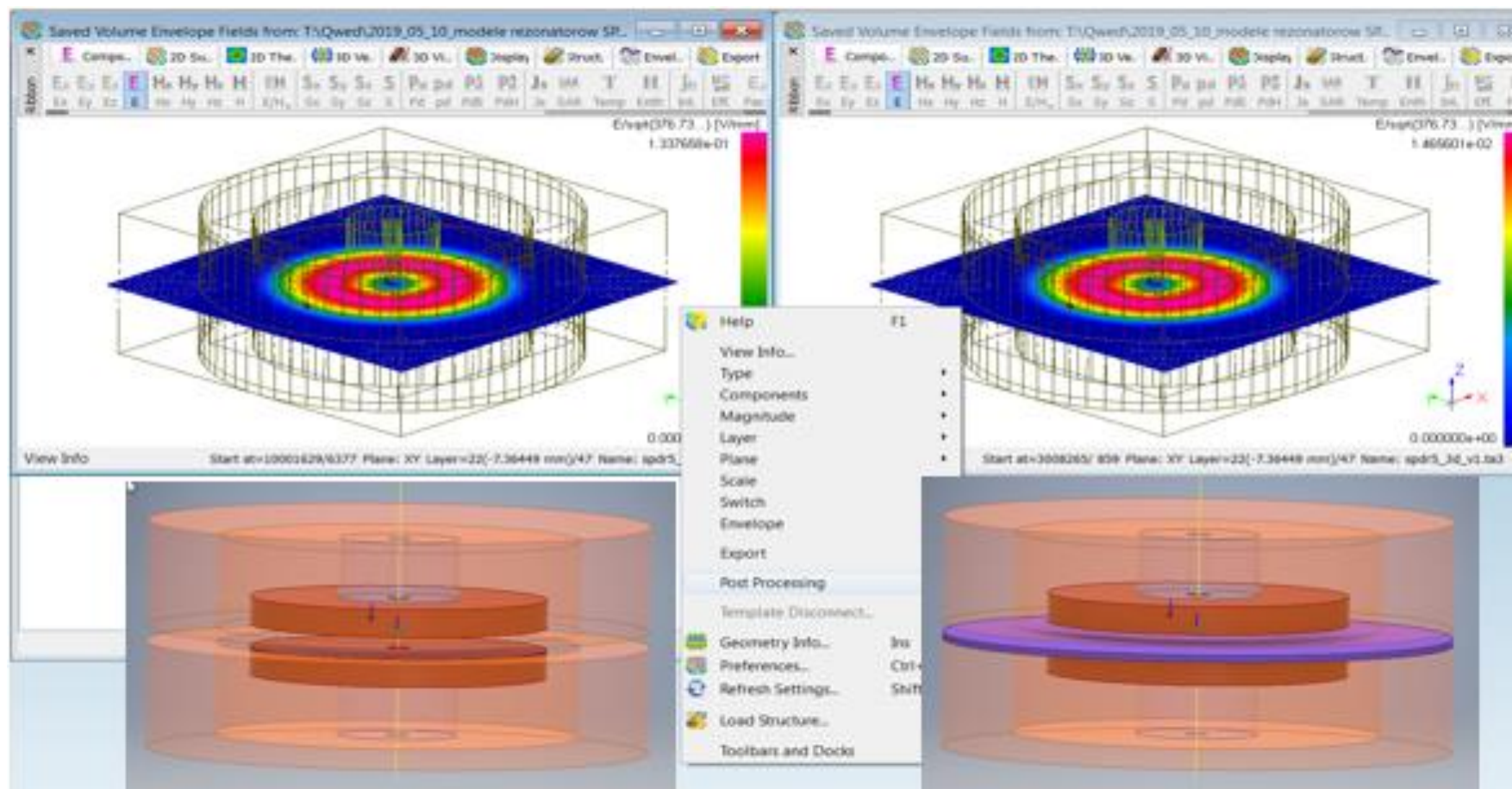


Sample in strong E-field nearly constant between the **two posts**

- applicable to thin sheets
- low sensitivity to sample positioning along the height of the slot



QuickWave model for SPDR loaded with sample

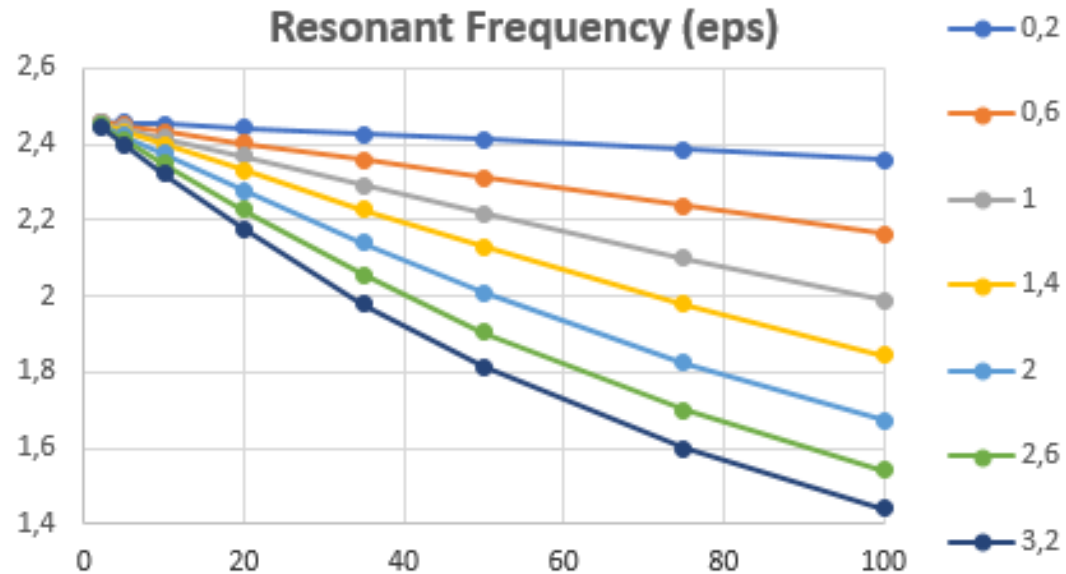


Field patterns remain practically unchanged
by **resonant frequencies** and **Q-factors** change,
providing information about **SUT** material parameters

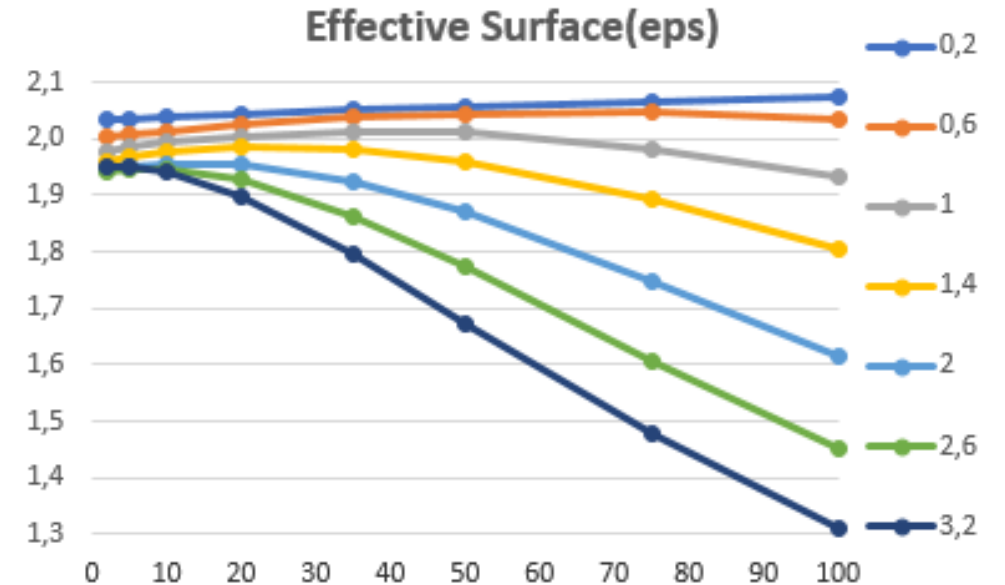


QuickWave model for SPDR loaded with sample

QuickWave simulations of 2.5GHz SPDR performed in automatic Parameter Sweep for varying sample thickness (colours) and dielectric constant (eps)



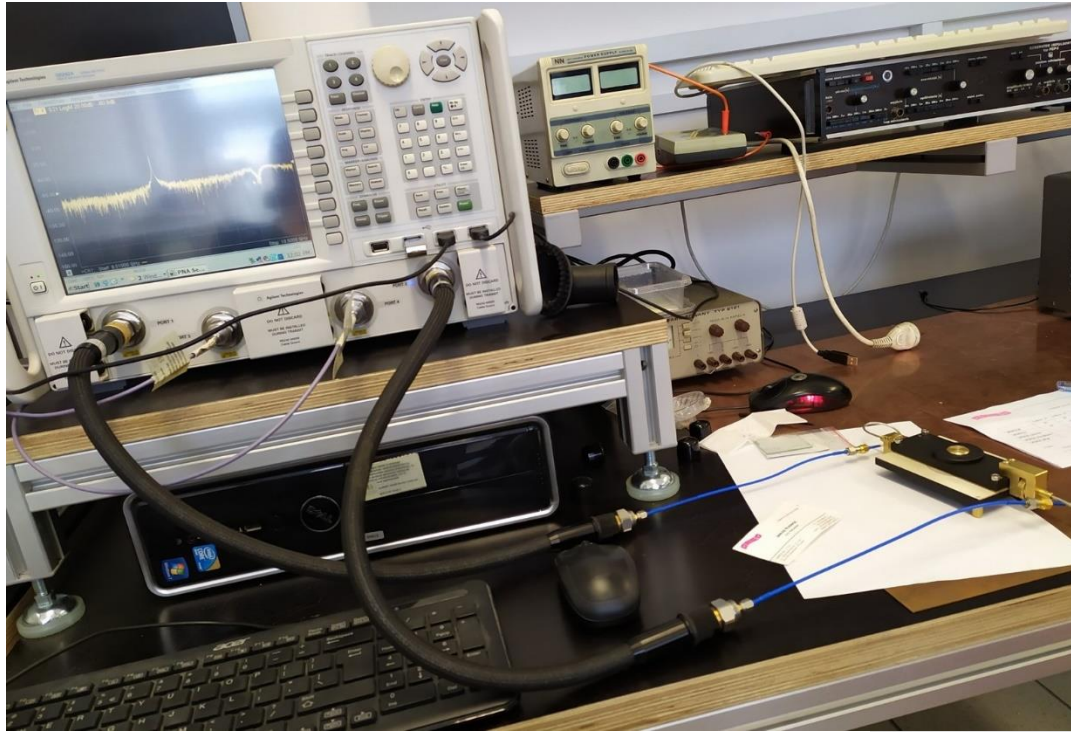
resonant freq. changes are nonlinear
(simple perturbation eqs. are not accurate enough)



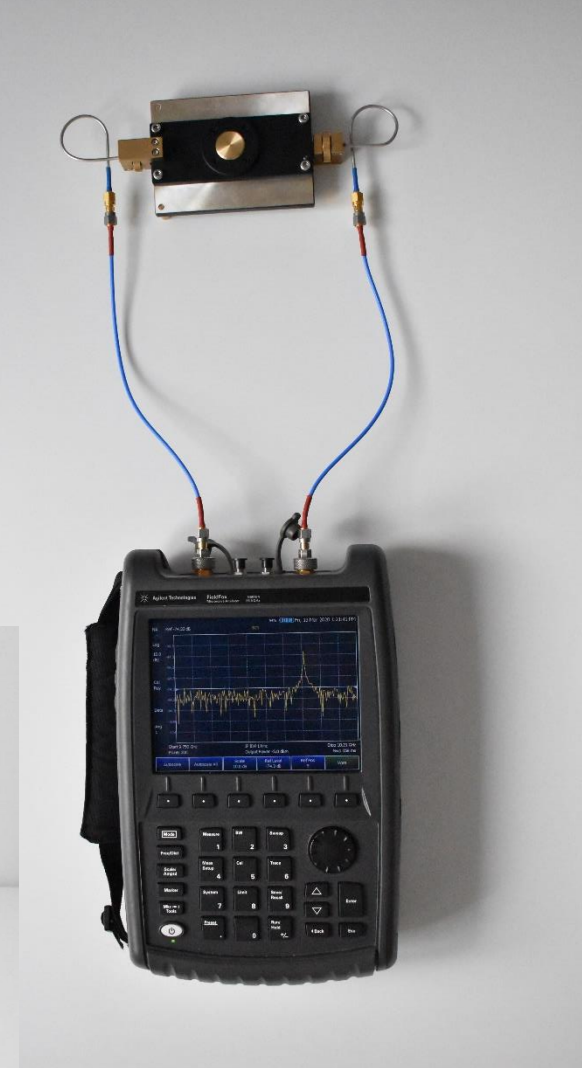
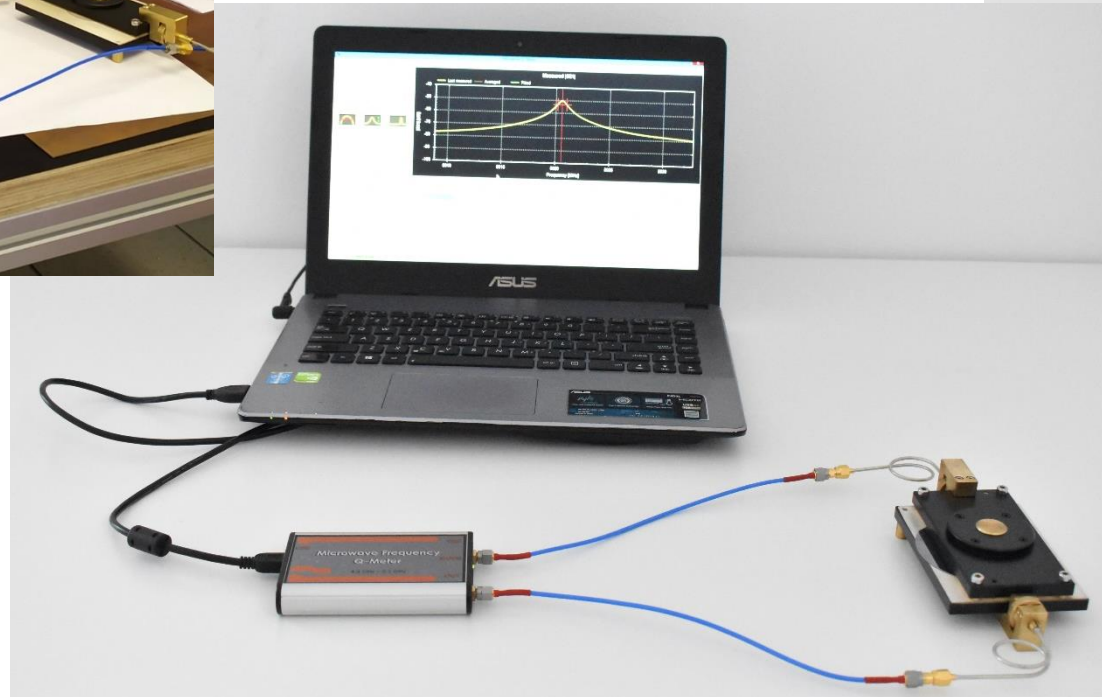
intermediate parameter is defined
leading to slowly-varying functions
tuned in calibration



SPDR use in big & small labs...



...and at home



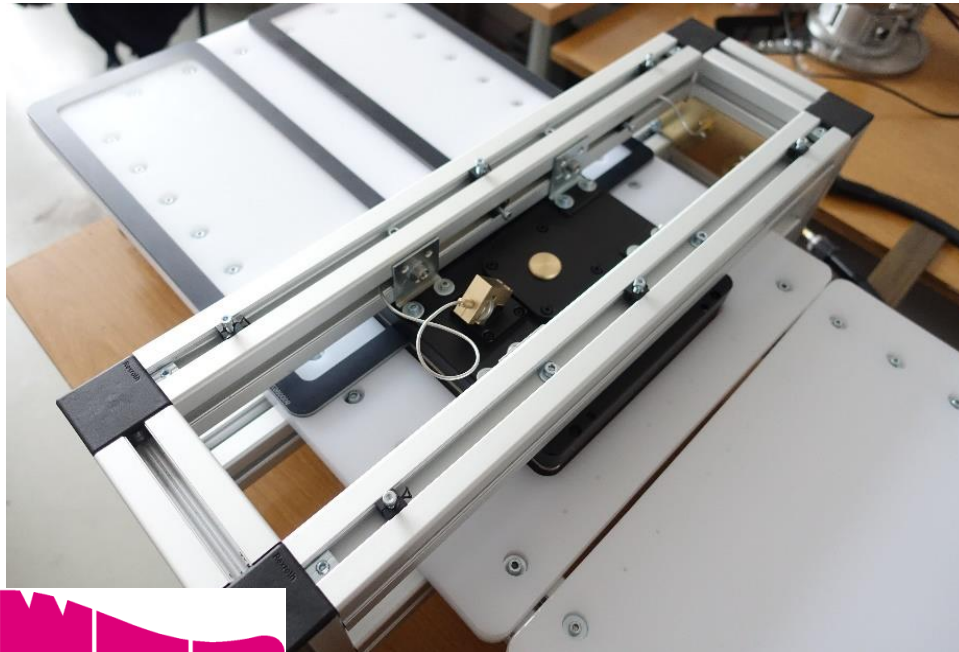
Surface scanning with SPDR

Obviating the limitations:

- SUT lateral **min size** ("absolute" EM constraint) - 14..120 mm
- spatial **resolution** 14..120 mm
- SUT lateral **max size** – 40..150 mm

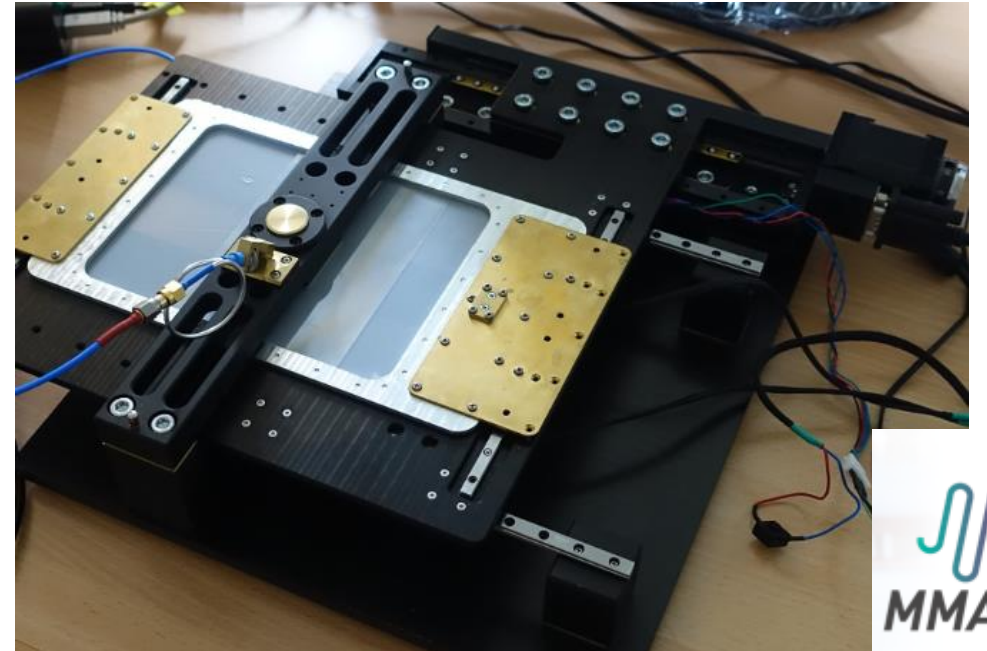
- **scanning & postprocessing**
- **scanning & postprocessing**
- **increase by change of mechanical construction**

manual scanner for large panes of glass
(MW oven window)

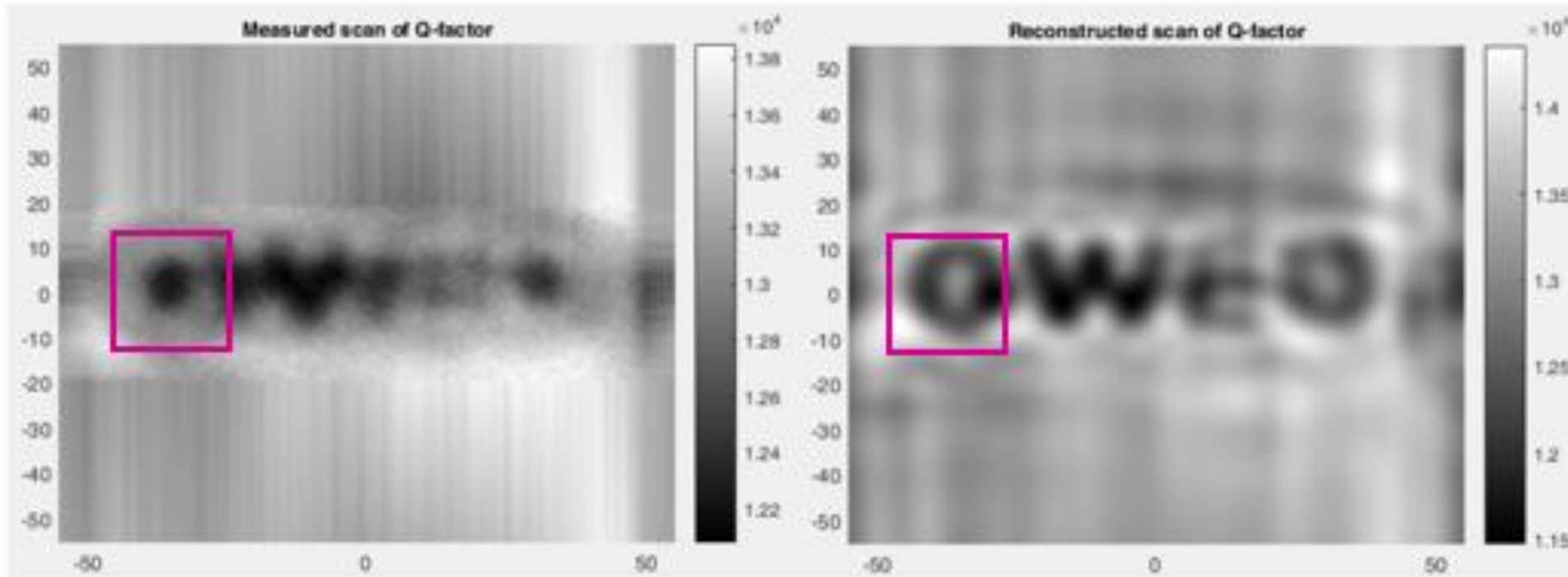


automatic scanner

semiconductor wafers, composites, ceramics

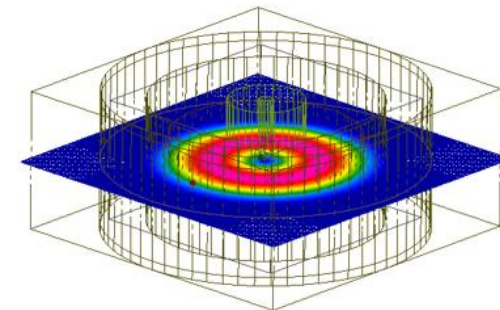
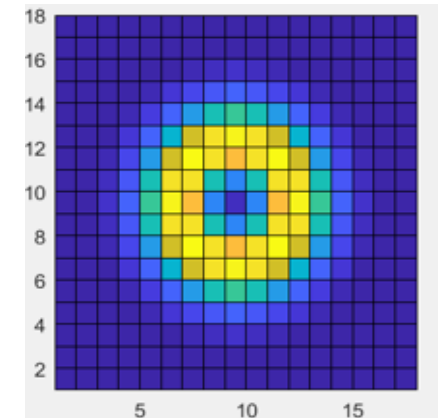


Surface scanning with SPDR & resolution enhancement



sample resistivity (measured Q-Factor)
scan with QWED 10GHz SPDR scanner
in H2020MMAMA project

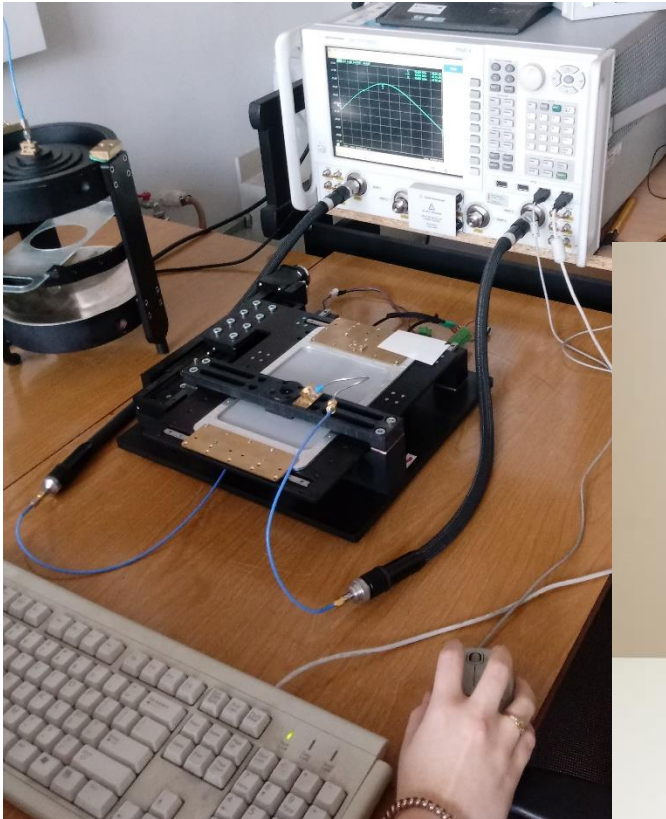
image post-processed
using SPDR field pattern
simulated in QuickWave



Patterned PEDOT:PSS sample courtesy MateriaNova, Belgium

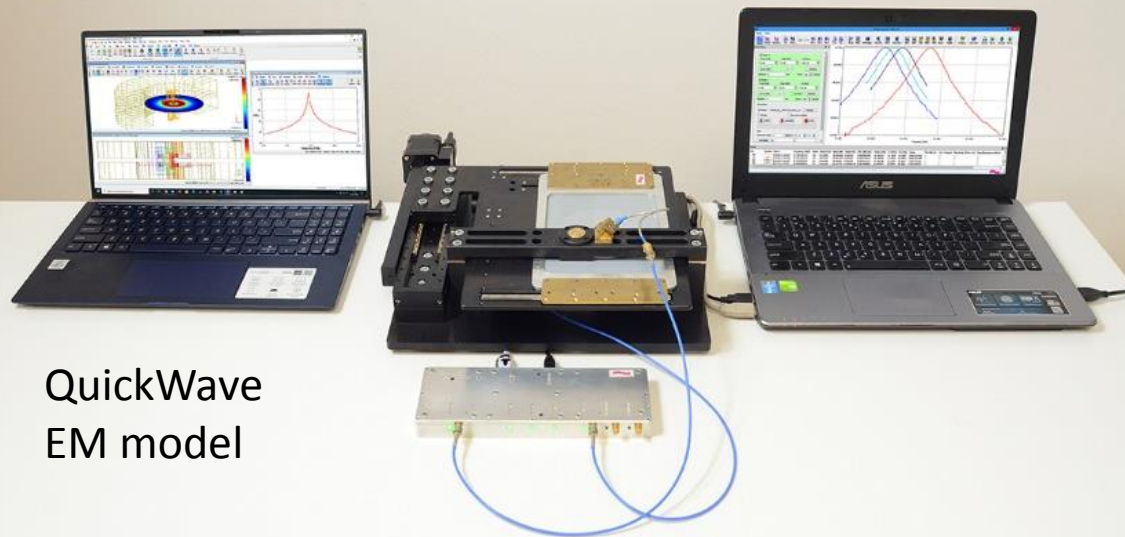


SPDR incorporated in 2D scanner (for surface non-uniformities)

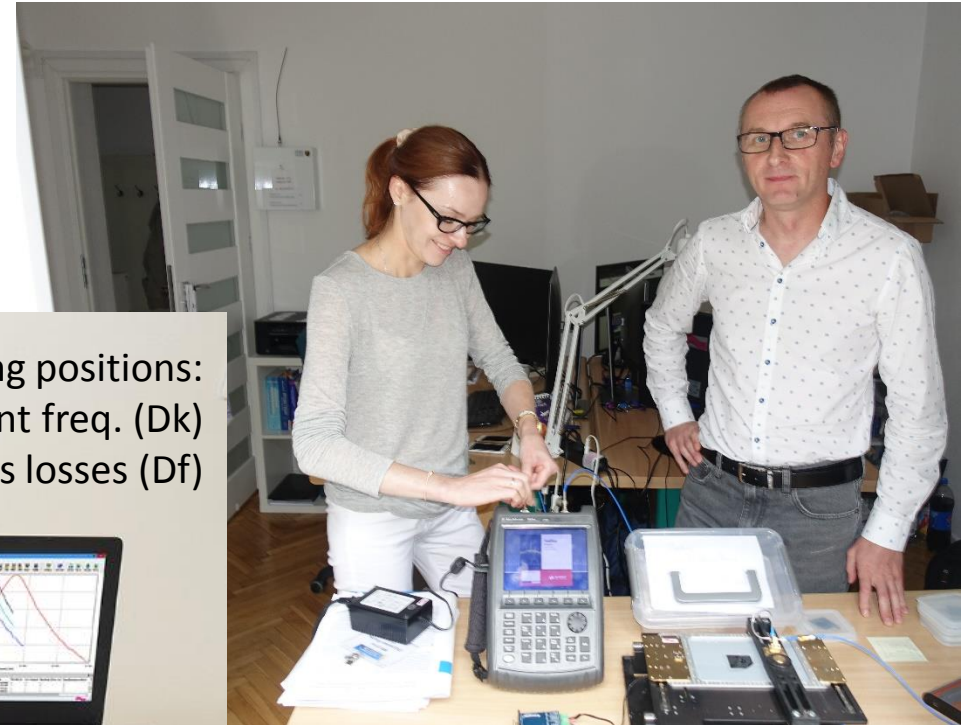


$|S_{21}|$ curves are for several scanning positions:

- curve max indicates resonant freq. (D_k)
- curve 3dB width indicates losses (D_f)



QuickWave
EM model



A joint product of QWED and Keysight, developed in the H2020 MMAMA project, has been acknowledged as **Innovation Radar** of the European research. It is also marked as **#Women led innovation**

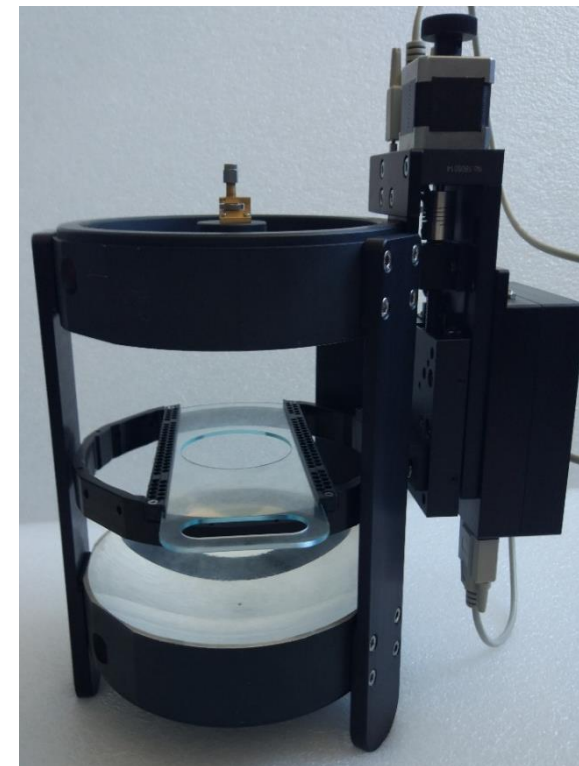
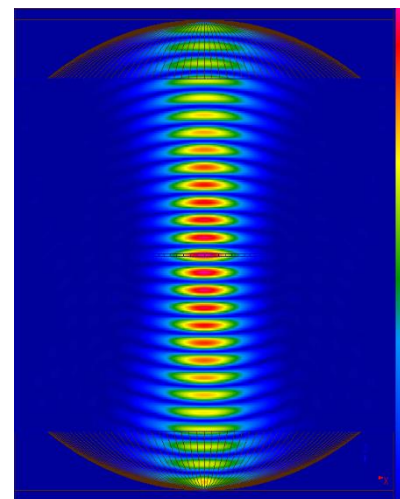
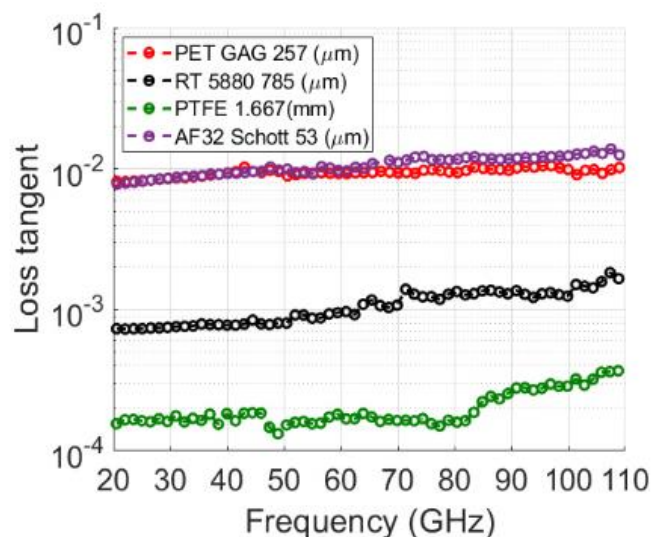
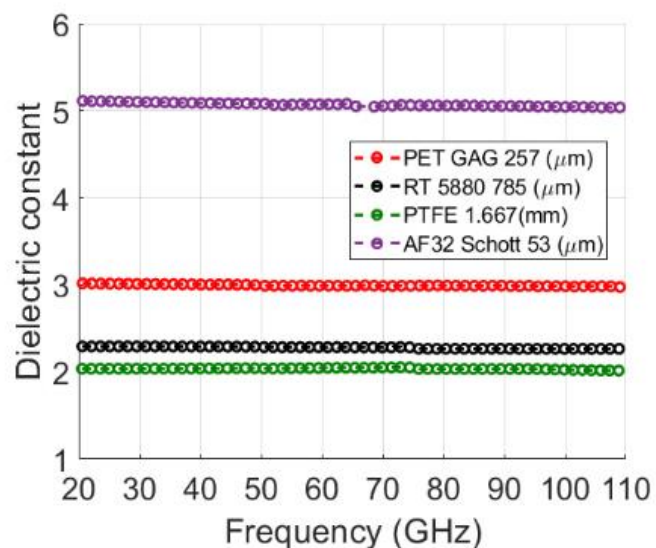
<https://www.innoradar.eu/resultbykeyword/qwed>



QuickWave design of mm-Wave resonators

- Standard SPDRs are provided for 1.1GHz – 15 GHz
- Custom designs feasible for 20 GHz, further limitation due to wavelength, manufacturing tolerances & losses
- Other resonator solutions (**FPOR, BCDR**) designed & recommended >15GHz

Fabry-Perot Open Resonator

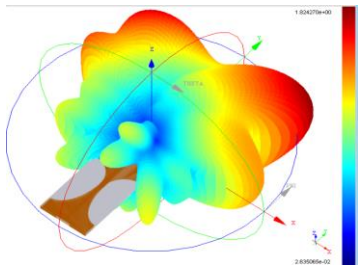


Fully automated wide-band multi-mode measurement: (10-15 min)

- Spectrum: 20-110 GHz
- Dk accuracy: $\Delta\epsilon/\epsilon < 0.5\%$
- Df range: $10^{-5} < \tan\delta < 10^{-2}$
- Sample diameter: > 3 inches
- Sample thickness: < 2 mm

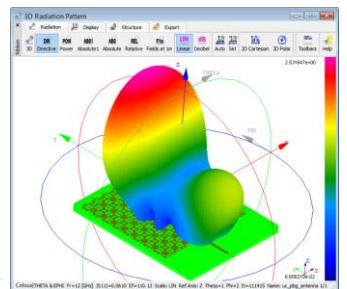


Antenna & feed systems design – for various applications

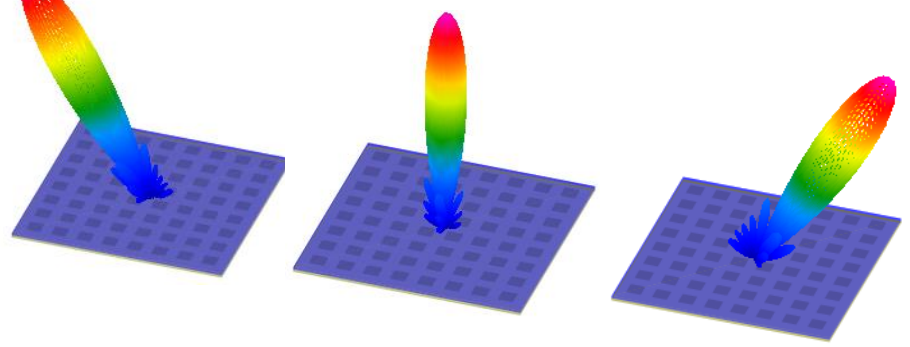


Balanced antipodal Vivaldi antenna & 3D radiation pattern at 10 GHz.

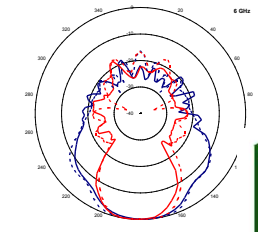
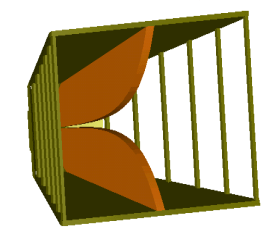
Aperture-coupled patch antenna on uniplanar photonic bandgap substrate & its radiation pattern at 12 GHz.



Antenna arrays for 5G and automotive radar application

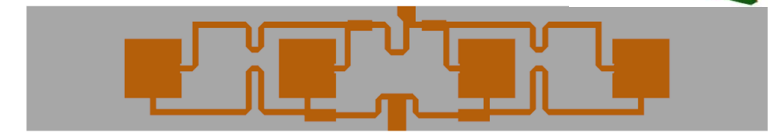


Designing and verifying tracking capabilities

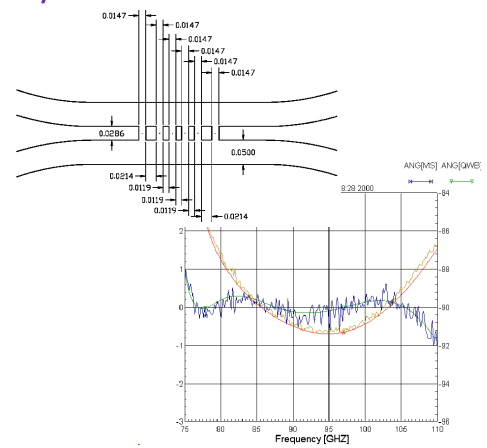


Pyramidal horn antenna for military surveillance measured (courtesy prof.B.Stec) & simulated patterns

Planar antennas for smart bio-sensors

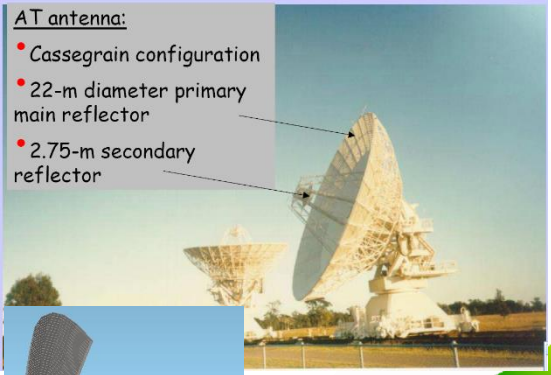


Antenna feed systems designed by NRAO



QuickWave 3D results at NRAO, see: ALMA Memos 381, 343, 325, 278.

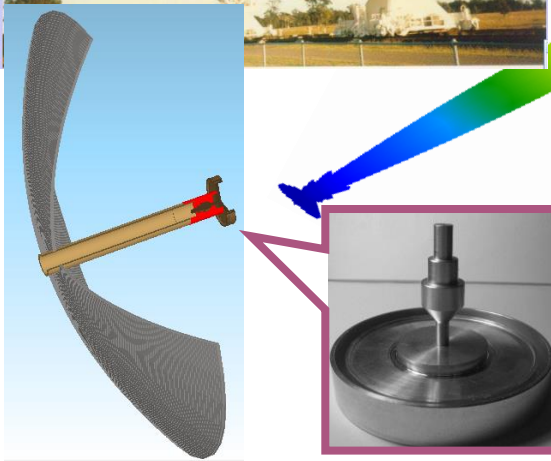
Large dual reflector antennas: Cassegrain, Gregorian, etc.



- AT antenna:
- Cassegrain configuration
 - 22-m diameter primary main reflector
 - 2.75-m secondary reflector

BOR FDTD

Unique, ultra-fast vector 2D Bessel & FDTD hybrid solver for design & analysis of devices with axial symmetry

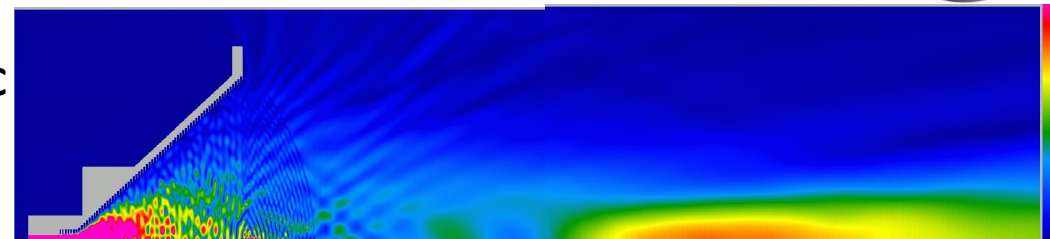


Scenarios modelled full-wave:

- 2500 λ on popular PC
- 5000 λ on top-shelf PC

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Smartwatch with embedded patch antenna

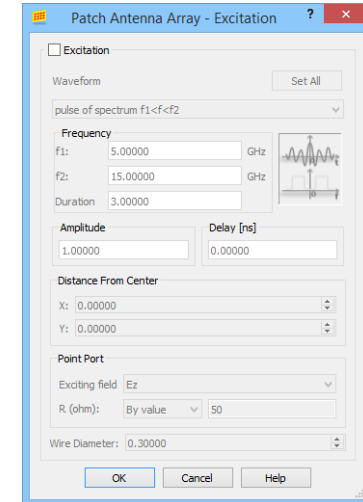
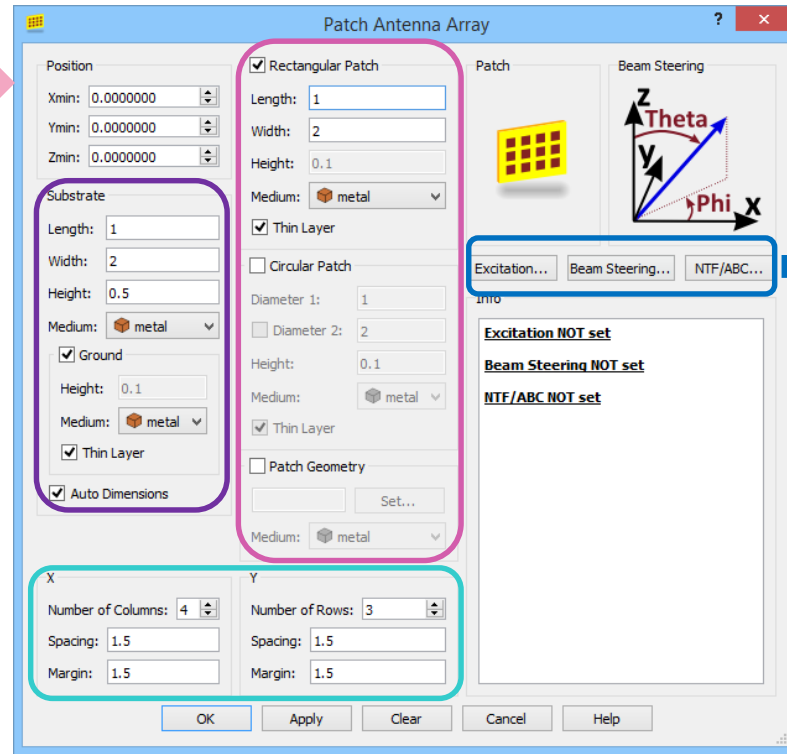
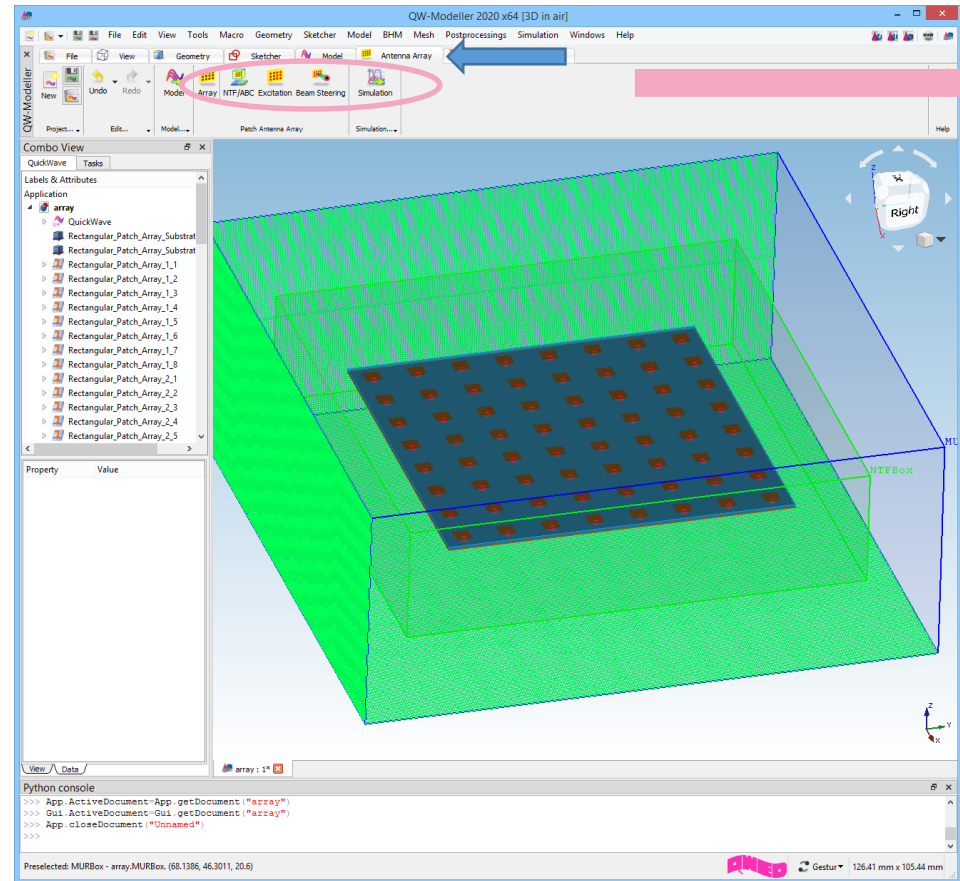


Corrugated horn antenna for material measurements



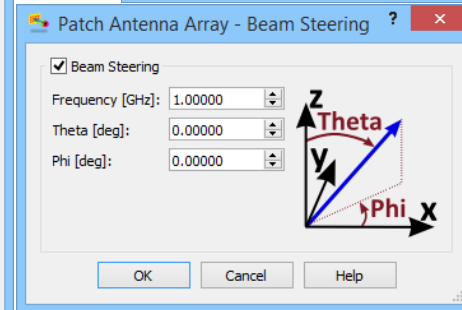
Dedicated wizards for 5G patch antenna array project creation

QW-Modeller

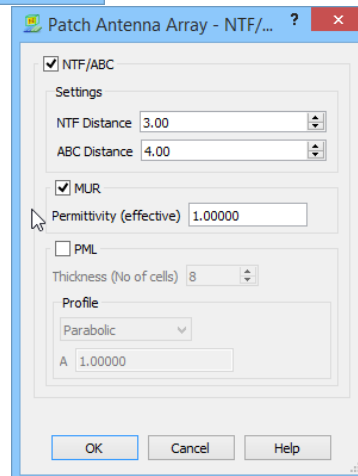


Feed parameters @ each patch

Automatic phase-shift adjustment between patches



User defined main beam angle



- ✓ Various patch shapes, incl. user-defined geometries
- ✓ Automatic substrate/ground inclusion, incl. dimensions auto-scaling
- ✓ Automatic matrix arrangement

Choice of suitable absorbing BC



Dedicated simulation & display regimes for 5G patch antenna analysis

Patch Antenna Array

Position
 Xmin: 0.0000000
 Ymin: 0.0000000
 Zmin: 0.0000000

Substrate
 Length: 1
 Width: 2
 Height: 0.5
 Medium: LTCC
 Ground
 Height: 0.1
 Medium: metal
 Thin Layer

Auto Dimensions

Rectangular Patch
 Rectangular Patch
 Length: 2.8
 Width: 2.8
 Height: 0.1
 Medium: metal
 Thin Layer

Circular Patch
 Circular Patch
 Diameter 1: 1
 Diameter 2: 2
 Height: 0.1
 Medium: metal
 Thin Layer

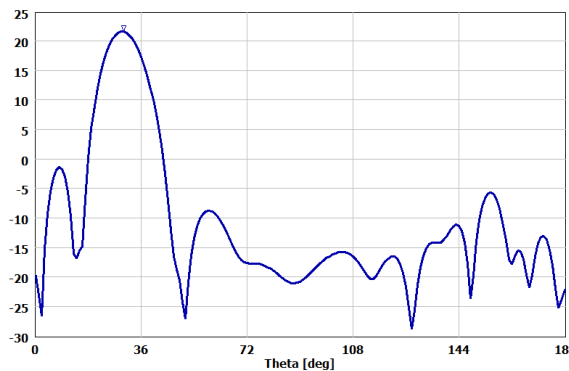
Patch Geometry
 Patch Geometry
 Medium: metal

Beam Steering
 Info
Excitation Info:
 Waveform: pulse: f1=26, f2=28
 Distance X From Center: 1
 Distance Y From Center: 0
 Exciting field: Ez
 Resistance: 50 [ohm]
 Wire diameter: 0.3
Beam Steering Info:
 Frequency: 27 [GHz]
 Theta: 30 [deg]
 Phi: 45 [deg]
NTF/ABC Info:
 NTF Distance: 5
 ABC Distance: 10
 ABC Type: MUR
 ABC MUR Permittivity: 1

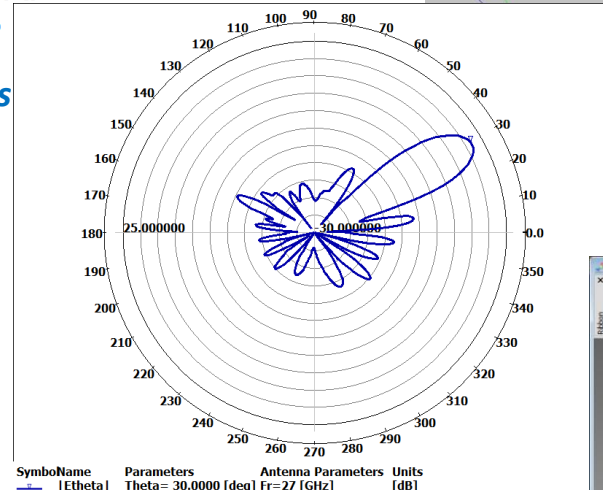
X
 Number of Columns: 8
 Spacing: 5
 Margin: 2

Y
 Number of Rows: 8
 Spacing: 5
 Margin: 2

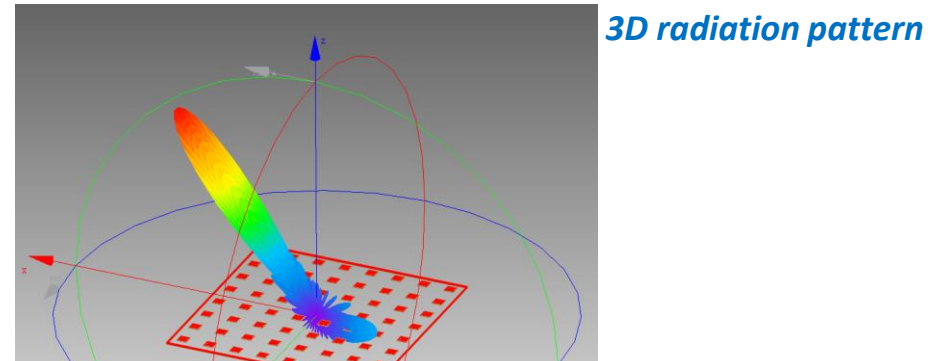
OK Apply Clear Cancel



2D radiation patterns



Distribution of source phase shifts across the array



3D radiation pattern

3D Radiation Pattern - Patch Antenna Array: Rectangular

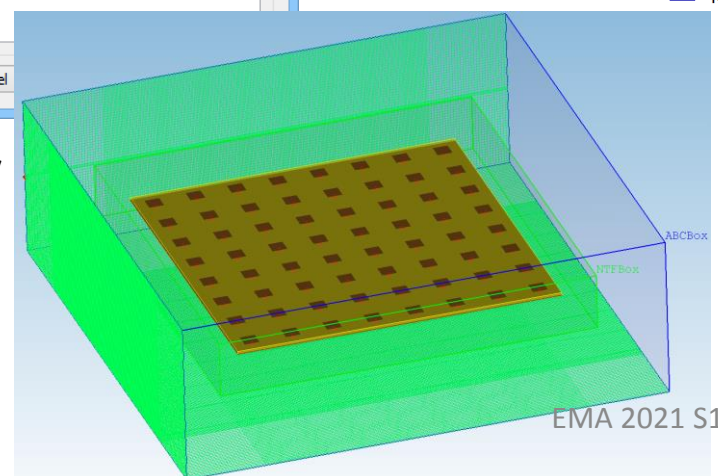
Amplitude Delay

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|---|---------|---------|---------|---------|---------|---------|---------|---------|
| 1 | 0 | 0.00919 | 0.01838 | 0.02758 | 0.03677 | 0.04596 | 0.05515 | 0.06435 |
| 2 | 0.00919 | 0.01838 | 0.02758 | 0.03677 | 0.04596 | 0.05515 | 0.06435 | 0.07354 |
| 3 | 0.01838 | 0.02758 | 0.03677 | 0.04596 | 0.05515 | 0.06435 | 0.07354 | 0.08273 |
| 4 | 0.02758 | 0.03677 | 0.04596 | 0.05515 | 0.06435 | 0.07354 | 0.08273 | 0.09192 |
| 5 | 0.03677 | 0.04596 | 0.05515 | 0.06435 | 0.07354 | 0.08273 | 0.09192 | 0.10112 |
| 6 | 0.04596 | 0.05515 | 0.06435 | 0.07354 | 0.08273 | 0.09192 | 0.10112 | 0.11031 |
| 7 | 0.05515 | 0.06435 | 0.07354 | 0.08273 | 0.09192 | 0.10112 | 0.11031 | 0.11950 |
| 8 | 0.06435 | 0.07354 | 0.08273 | 0.09192 | 0.10112 | 0.11031 | 0.11950 | 0.12869 |

Patch Type: Rectangular
 Beam Steering
 Phi [deg]: 45.00
 Frequency [GHz]: 27.00
 Theta [deg]: 30.00

OK Apply Cancel Help

LTCC-based 8x8 patch array



Modelling EM field interaction with tissues

Recent research
on 5G safety
June 2020

Absorption of 5G Radiation in Brain Tissue as a Function of Frequency, Power and Time

IEEE Access
Multidisciplinary | Rapid Review | Open Access Journal

DAVID H. GULTEKIN^{1,2} AND PETER H. SIEGEL^{2,3,4}, (Life Fellow, IEEE)

¹Zuckerman Mind Brain Behavior Institute, Columbia University, New York City, NY 10027, USA

²THz Global, La Cañada Flintridge, CA 91011, USA

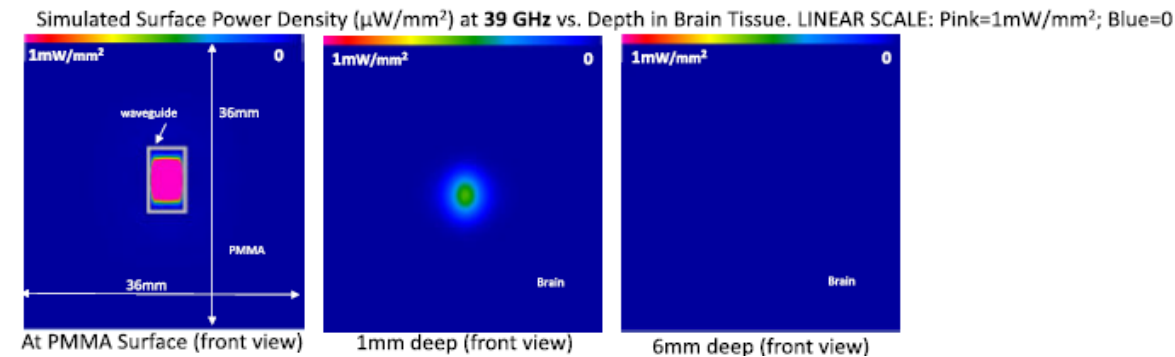
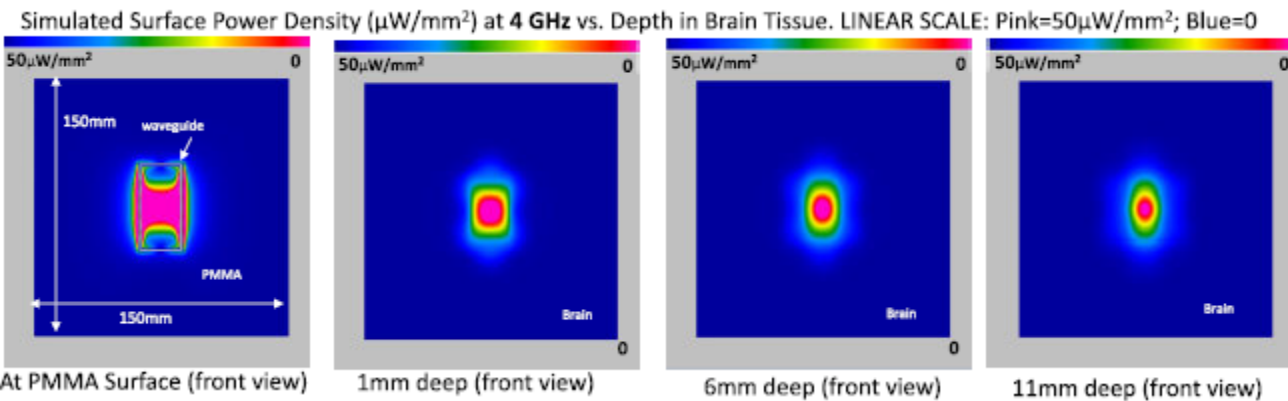
³Jet Propulsion Laboratory, National Aeronautics and Space Administration, Pasadena, CA 91109, USA

⁴Department of Electrical Engineering, California Institute of Technology, Pasadena, CA 91125, USA

QuickWave modelling applied
to interpret laboratory experiments
with bovine tissue irradiation

4 GHz

39 GHz

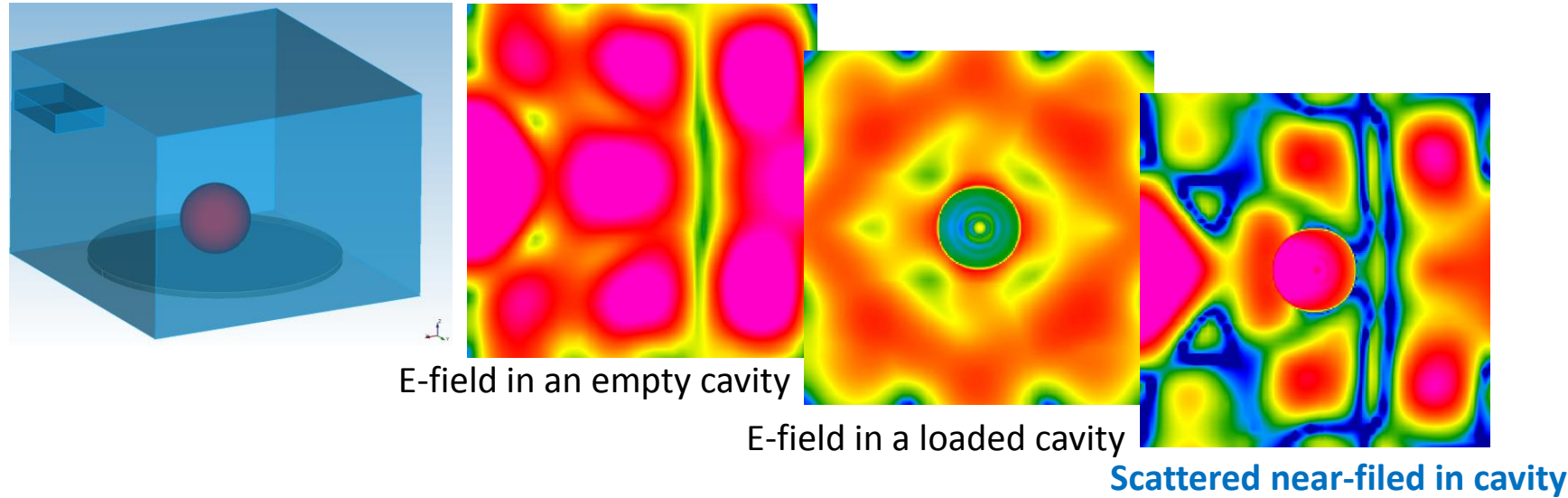


Using 1W of incident power,
an average power density of 138, 613 and 16 578 W/m^2 (at 1.9, 4, 39GHz, respectively)
is derived at the tissue surface.

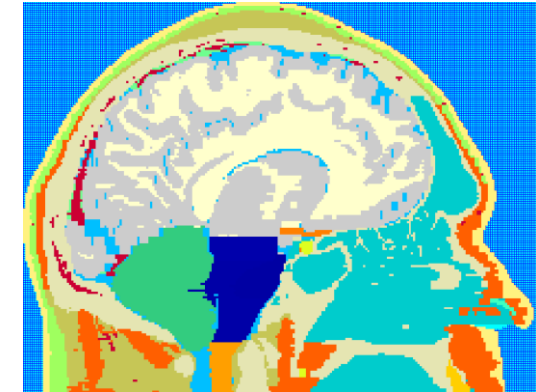


Modelling EM field interaction with tissues

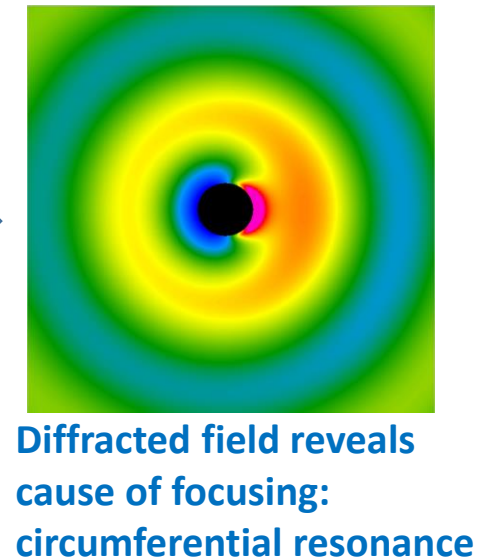
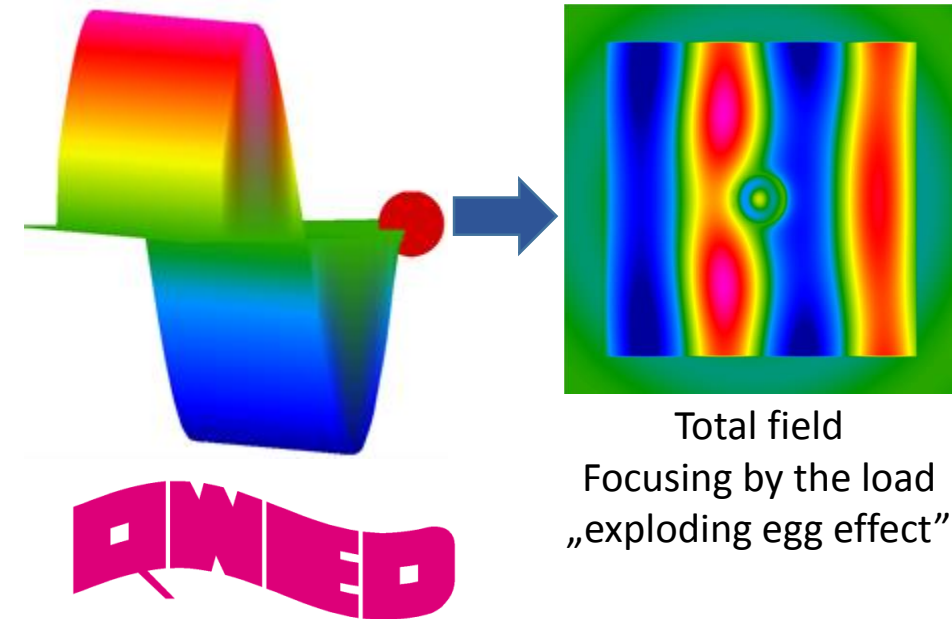
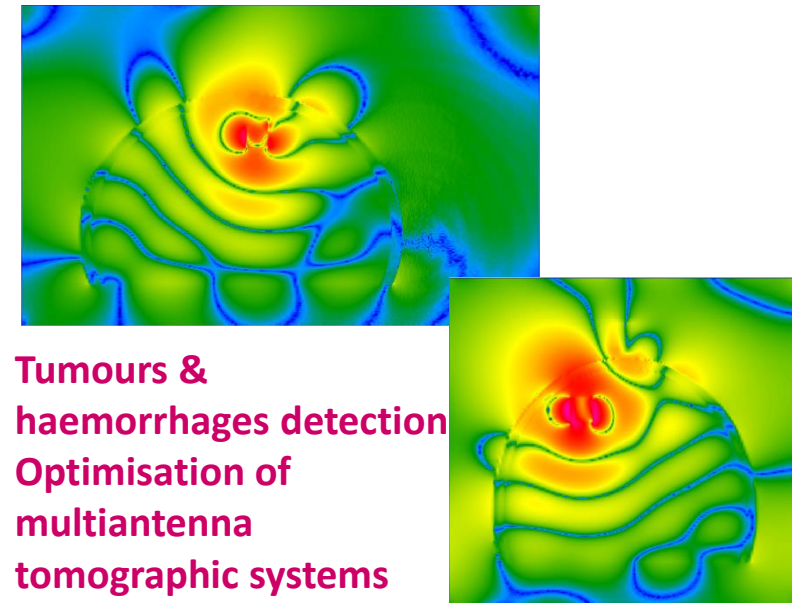
Separation of incident and diffracted fields (*option implemented per request of P.O.Risman, Malardalen Univesity*)



Detection of inhomogenities in tissues



AustinMan model*
converted to
QuickWave EM
software for
Mälardalen
University, Sweden



EMA 2021 S13, 22 Jan 2021

* <https://sites.utexas.edu/austinmanaustinwomanmodels/>

Acknowledgements

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research and innovation programme

under grant agreement

NanoBat No 861962.

(website: www.nanobat.eu)



Simulations conducted with **QuickWave EM software**, developed & commercialised by QWED.

The original designs of QWED resonators for material measurements from Prof. Jerzy Krupka, e.g.:

J. Krupka, A. P. Gregory, O. C. Rochard, R. N. Clarke, B. Riddle, and J. Baker-Jarvis, "Uncertainty of complex permittivity measurements by split-post dielectric resonator technique", *J. Eur. Ceramic Soc.*, vol. 21, pp. 2673-2676, 2001.

J. Krupka and J. Mazierska, "Contactless measurements of resistivity of semiconductor wafers employing single-post and split-post dielectric-resonator techniques," *IEEE Trans. Instr. Meas.*, vol. 56, no. 5, pp. 1839-1844, Oct. 2007.

Scenarios of microwave medical applicators from Per O. Risman, Microtrans AB & Malardalen University, Sweden.

Conclusions

With this talk we seek collaborations:

on the development of:

- material measurement **test-fixtures**,
- **applicators** for processing of materials,
- **software** models & workflows
for 5G materials & applications.

on behalf of:

- **QWED** team,
- our **European project NanoBat**,
- members of broader EU initiatives, e.g.
European Materials Modelling Council.



THANK YOU!

...and hoping to talk to you in person next year...

